

CHEMICAL DURABILITY OF GLASS

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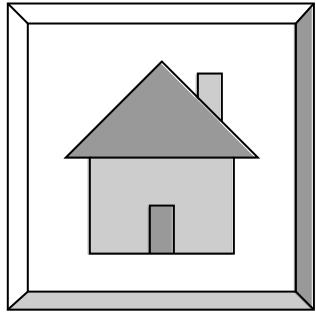
Department of Materials Science, Faculty of Science, Chulalongkorn University

&

**Department of Science Service
Bangkok 14th September 2010**

conradt@ghi.rwth-aachen.de



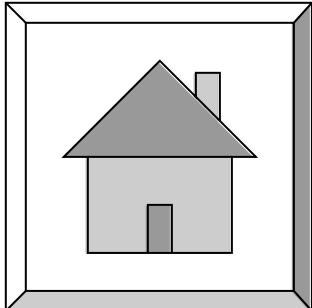


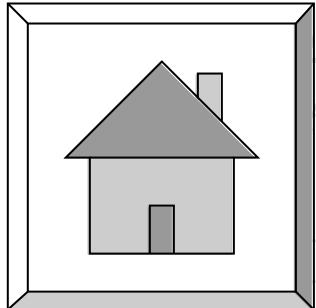
= load down & read at home

data sources

AQUEOUS SYSTEMS

- Pourbaix: Atlas of Electrochemical Equilibria in Aqueous Solutions
aq. pH-Eh speciation of the entire periodic table of elements
- Iler: The Chemistry of Silica (1979) *more than 2600 references!*
- Baes & Mesmer: The thermodynamics of cation hydrolysis (1981)
- Brinker & Scherer: Sol-Gel Science (1990)
- H.E. Bergna: The colloid Chemistry of Silica (1994)
- G. Sposito: The Environmental Chemistry fo Alumina (1996)





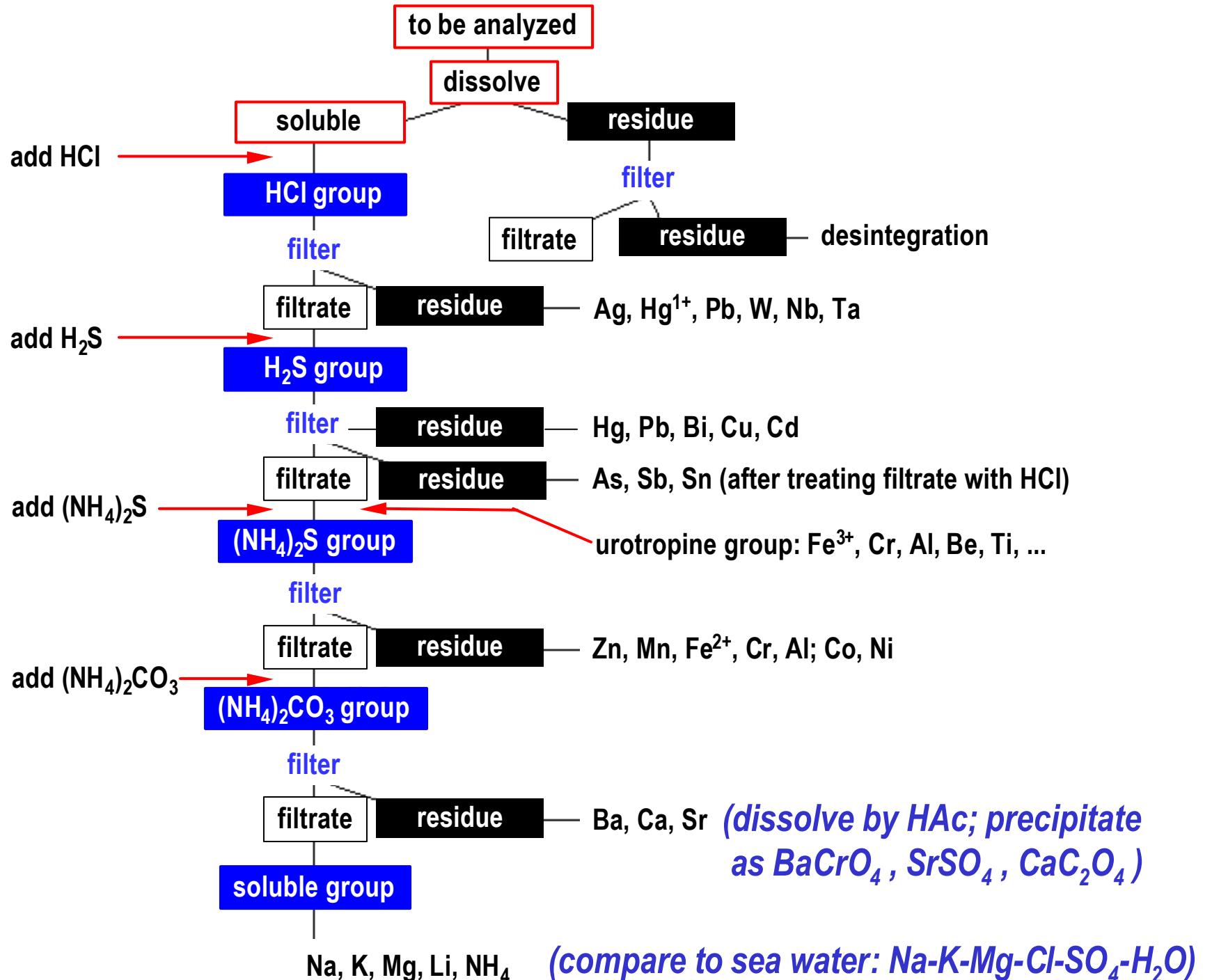
SYSTEMS

Atlas of Electrochemical Equilibria in Aqueous Solutions
speciation of the entire periodic table of elements
Chemistry of Silica (1979) *more than 2600 references!*

- Baes & Mesmer: The thermodynamics of cation hydrolysis (1981)
- Brinker & Scherer: Sol-Gel Science (1990)
- H.E. Bergna: The colloid Chemistry of Silica (1994)
- G. Sposito: The Environmental Chemistry fo Alumina (1996)

GLASS CORROSION

- ICG compilation of literature (1972) *almost 1000 references!*
- Holland (1964)
- Besborodow (1972)
- Clark, Pantano & Hench (1979)
- Doremus & Tomozawa (1977-82)
- Scholze (1964-91)
- Paul (1982)
- Clark & Zois (1992)

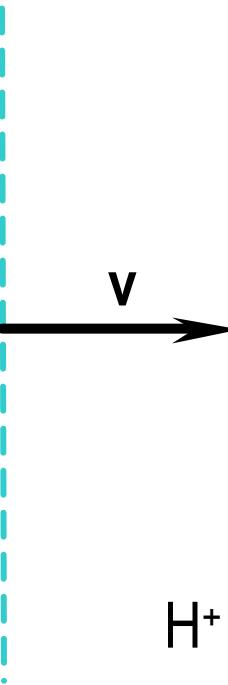
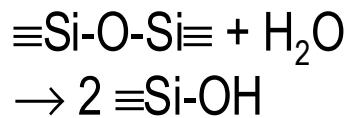
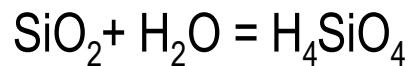


phenomena observed

standard model

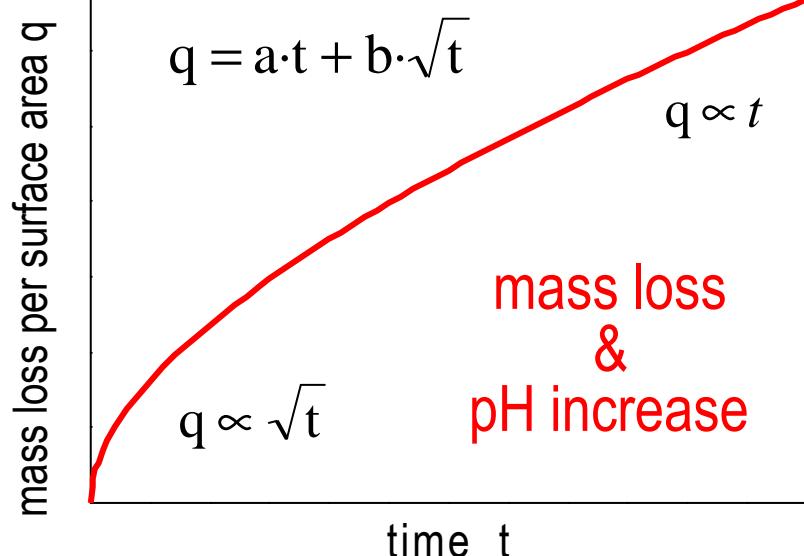
glass surface at $t = 0$

network dissolution
 $(q \propto t)$

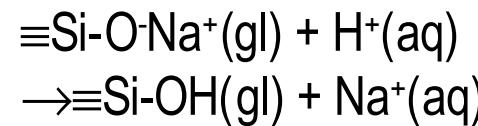


ion exchange zone

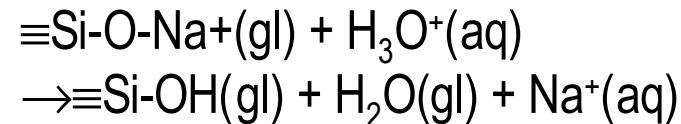
bulk glass



leaching
 $(q \propto \sqrt{t})$

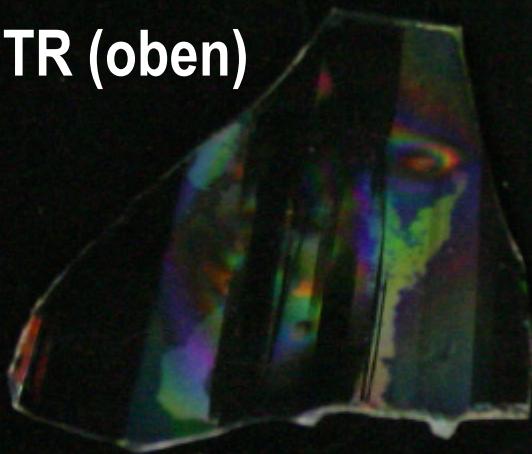


or



Korrosionslösung: Spülmittel A		
27	35	43
27A	35A	43A
Glas 1-1	Glas 2-1	Glas 3-1

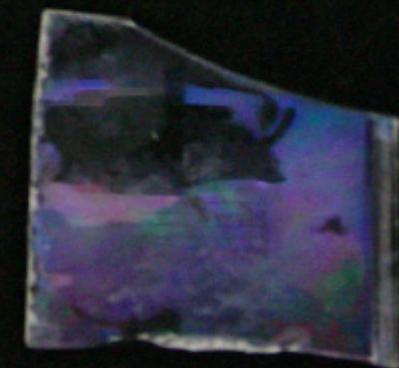
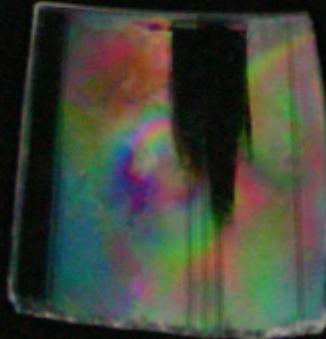
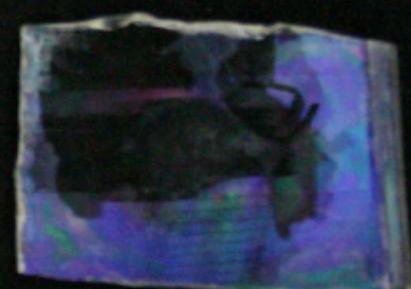
TR (oben)

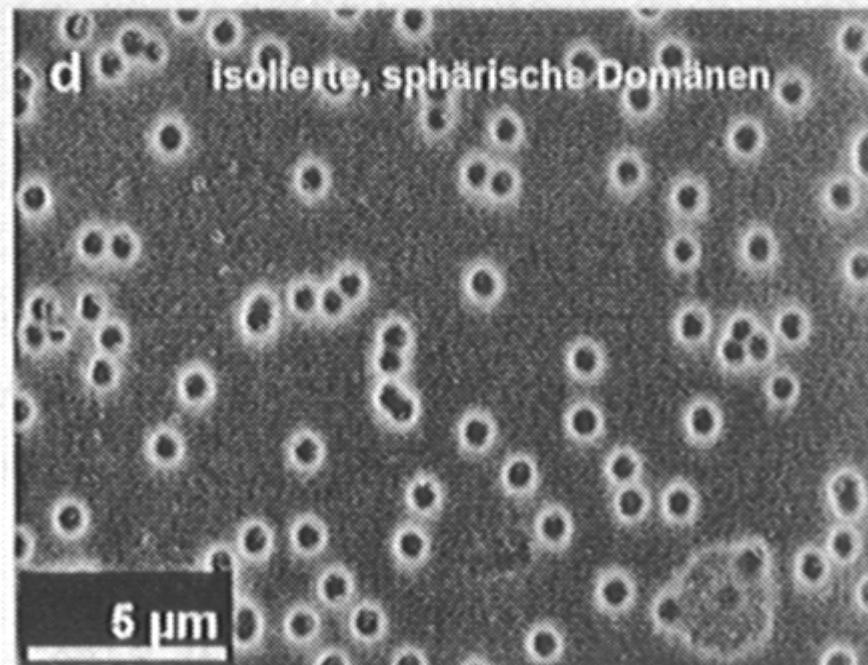
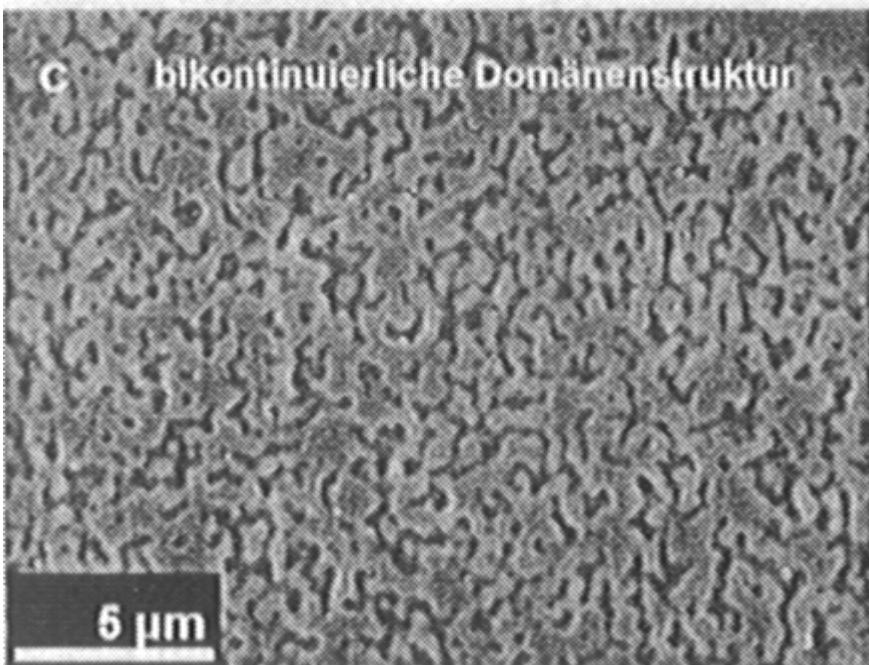
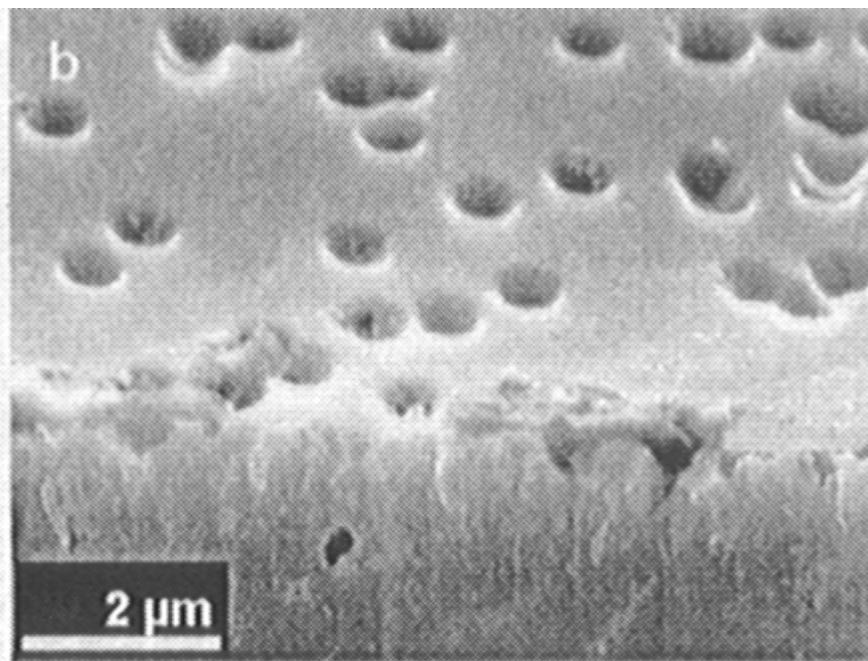
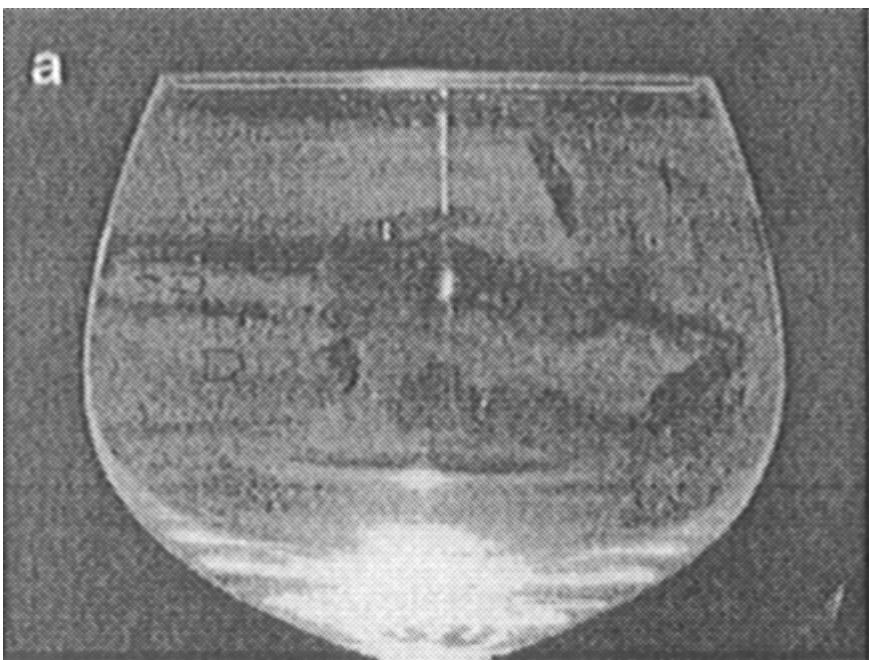


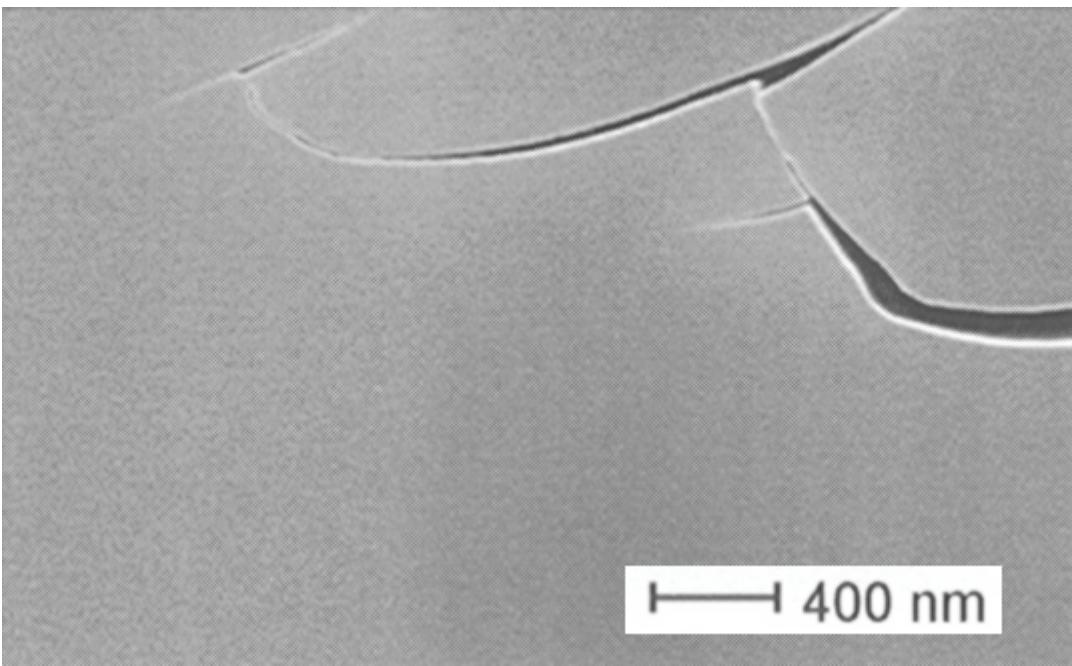
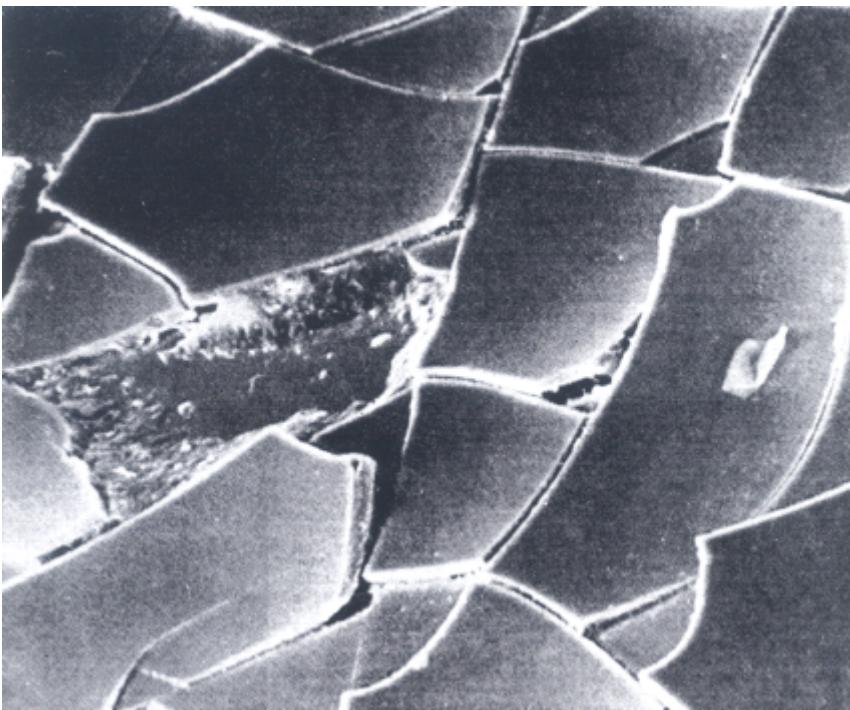
RIE (oben)

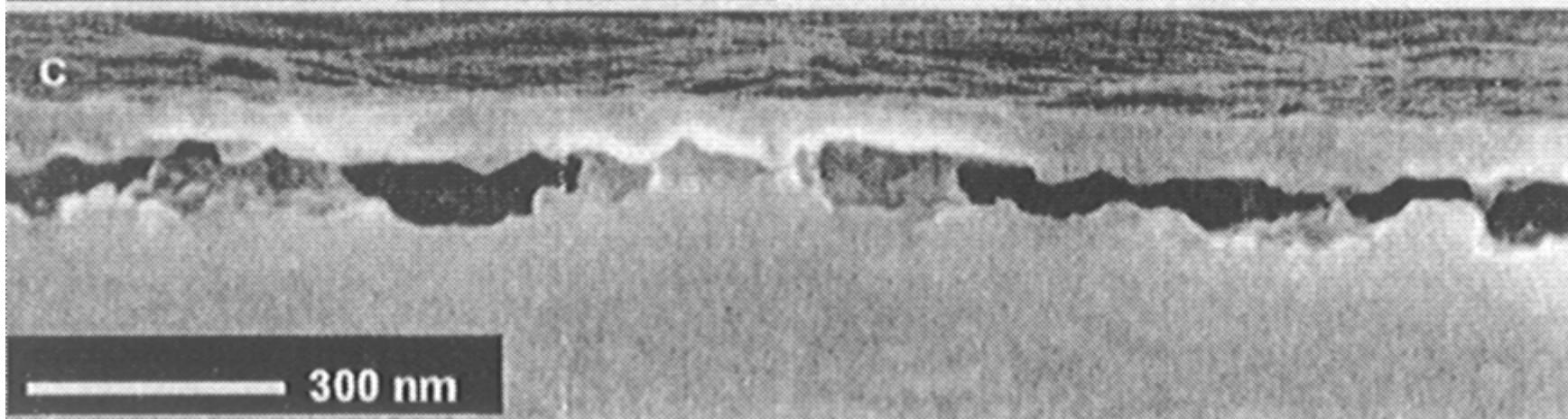
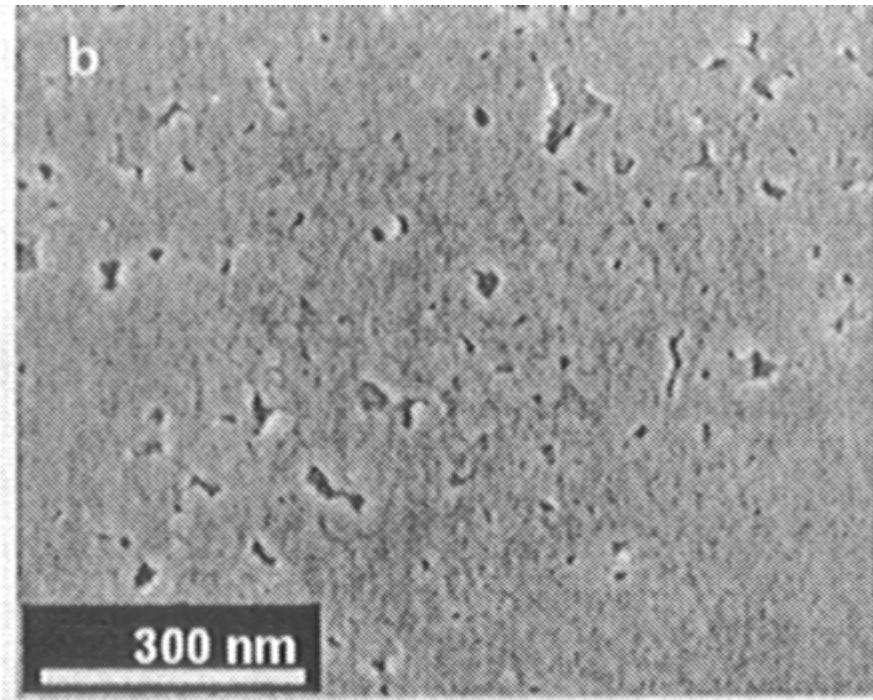


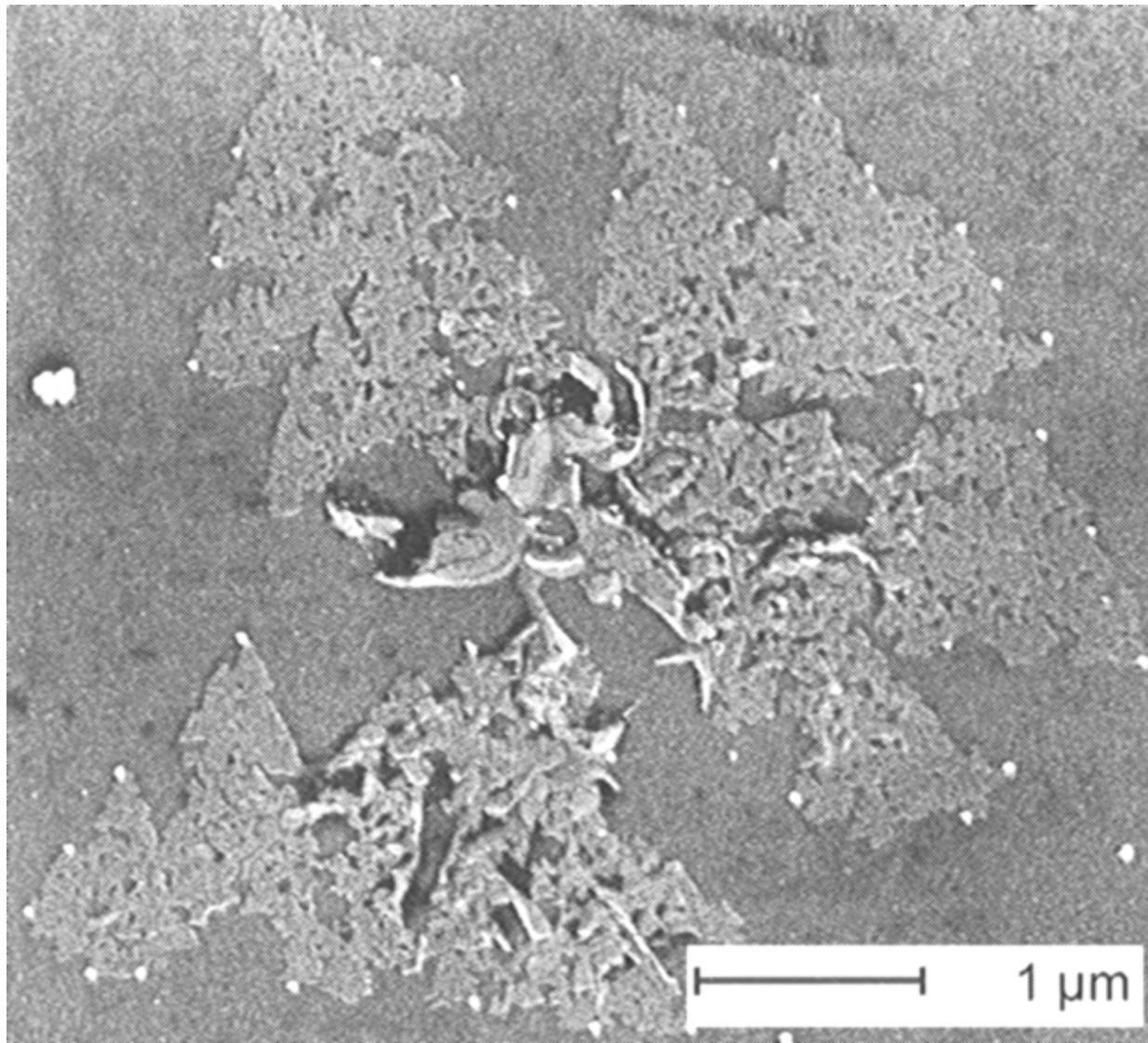
OC (oben)

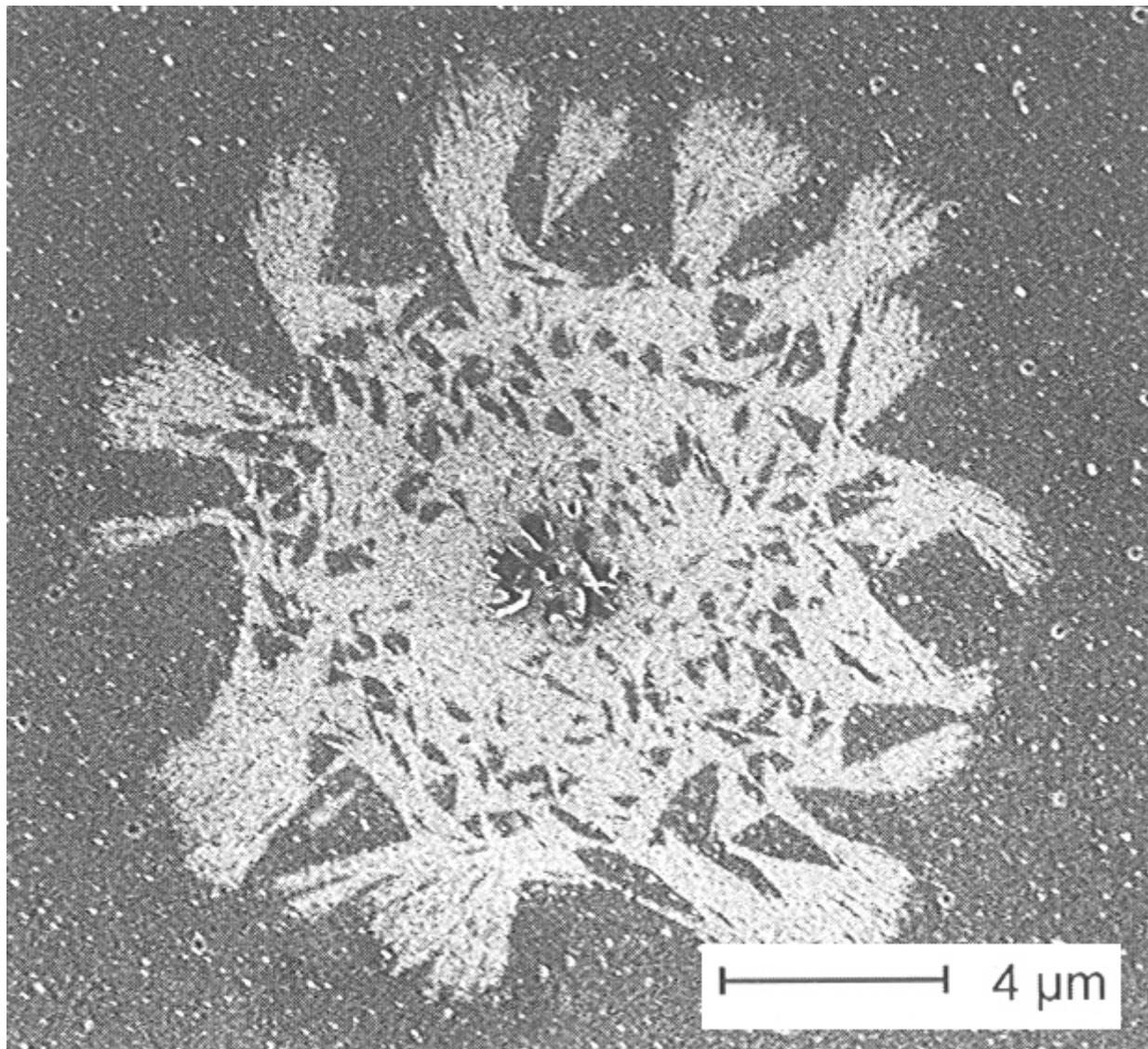




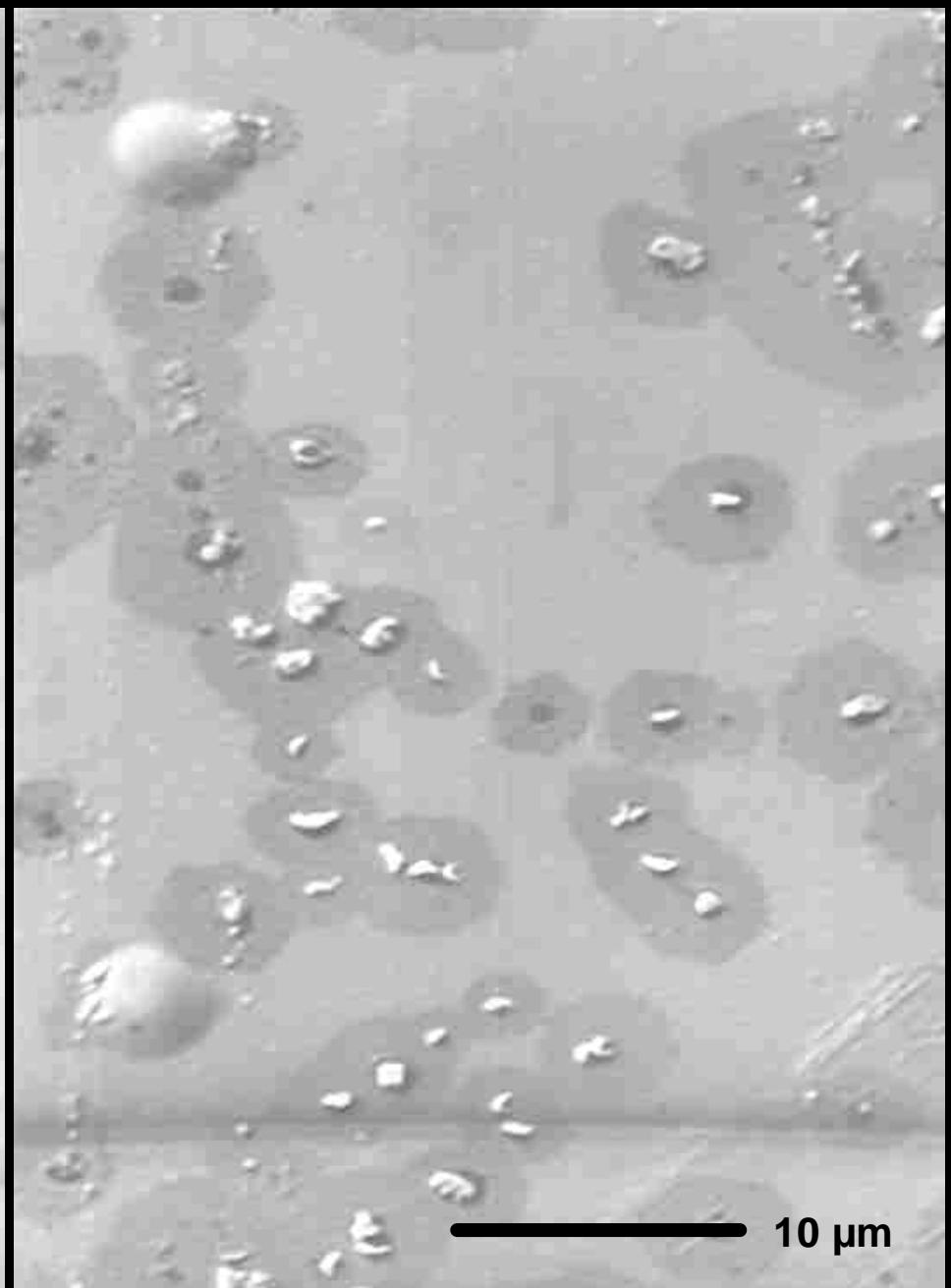




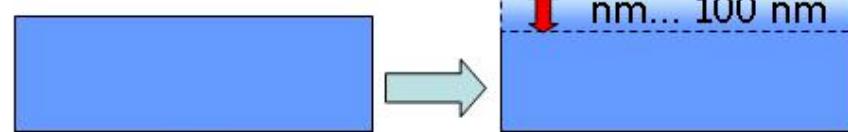




„soda bloom“ on OCEAN-Glas

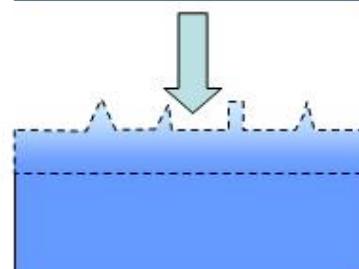


vertical differentiation:

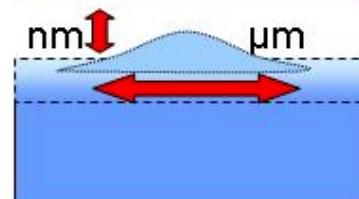


lateral differentiation:

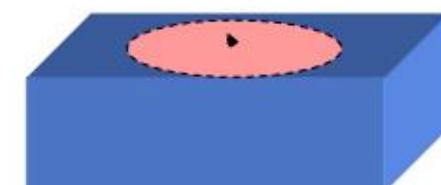
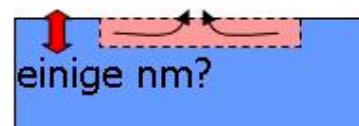
emerging surface
roughness



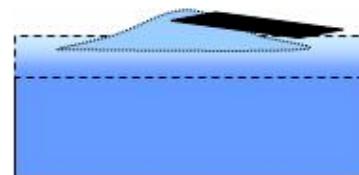
local swelling



lateral diffusion
zones



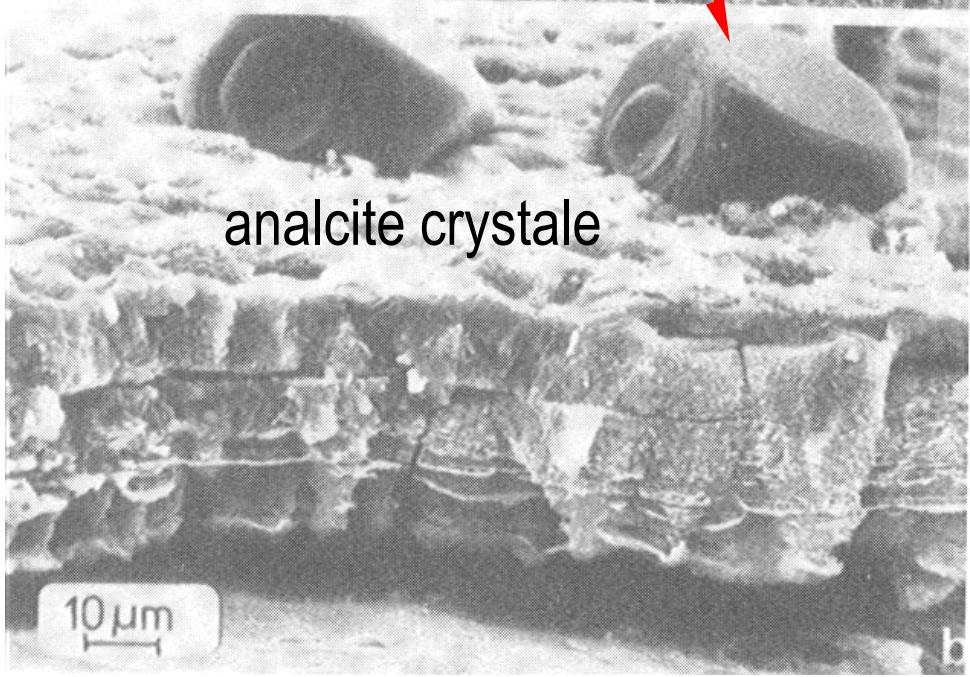
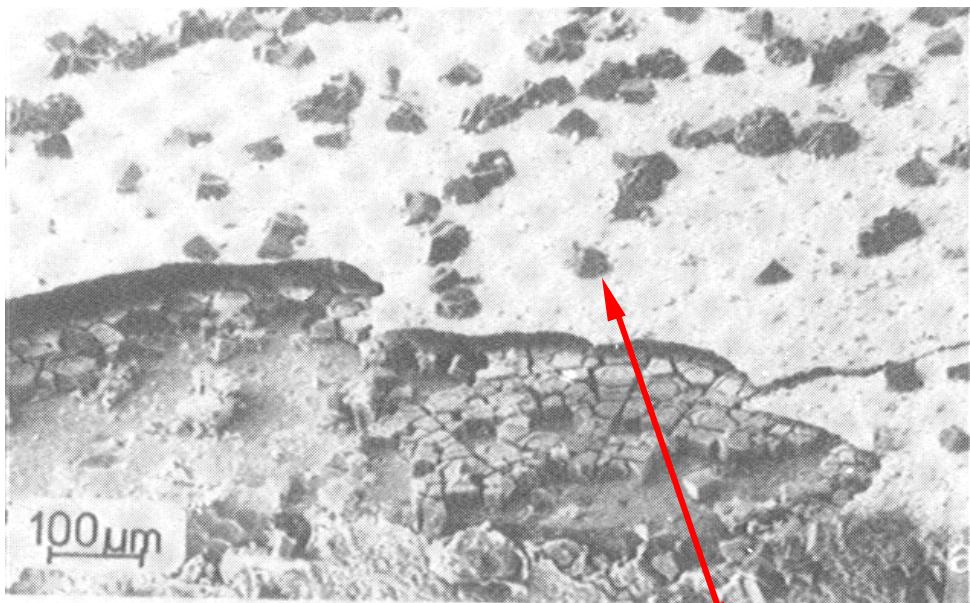
crystallization



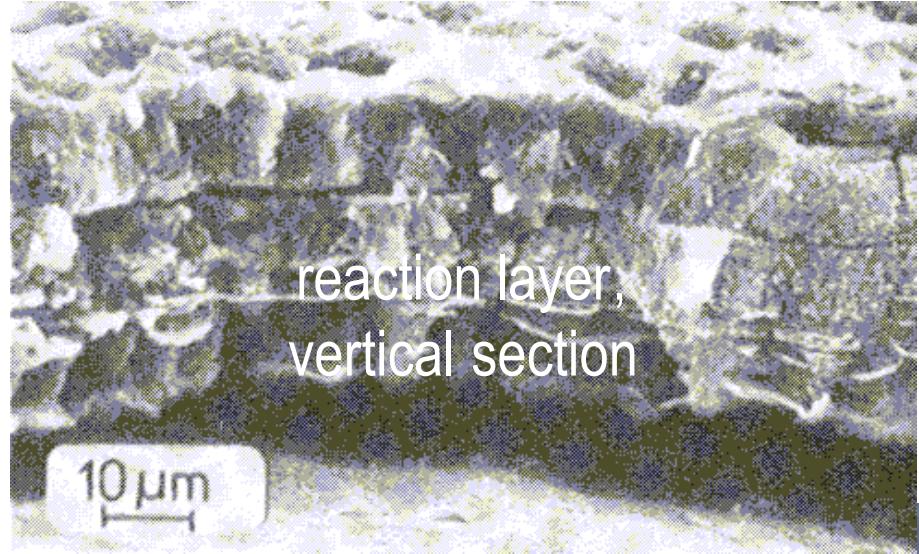
pitting



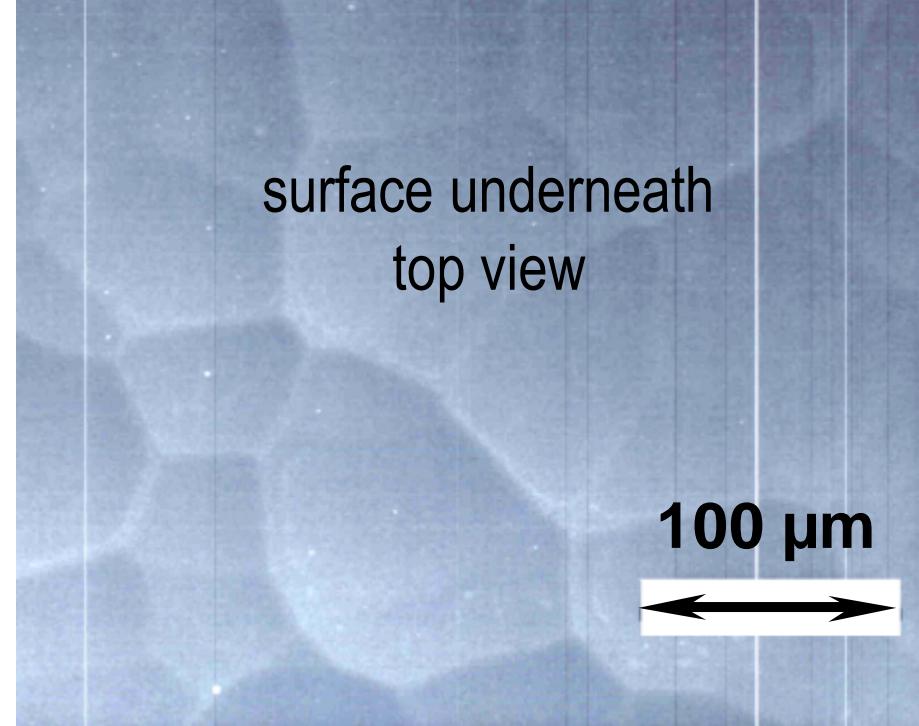
after: E. Rädlein



analcite crystals



reaction layer,
vertical section



surface underneath
top view

100 μm
↔

mineralized glass,
amorphous and crystalline precipitates,
„back precipitates“, „transformed layer“

adsorbed layer

surface zone

aqueous solution,
dissolved glass
components

bulk glass

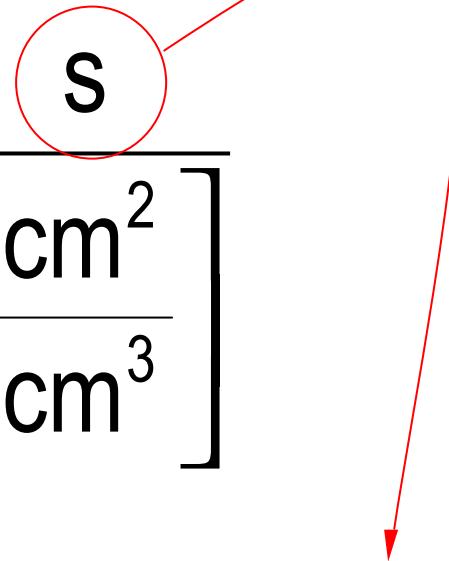
aqueous system

residual glass

standards

static tests

$$\frac{c}{\left[\frac{g}{cm^3} \right]} = \frac{q}{\left[\frac{g}{cm^2} \right]} \cdot \frac{s}{\left[\frac{cm^2}{cm^3} \right]}$$

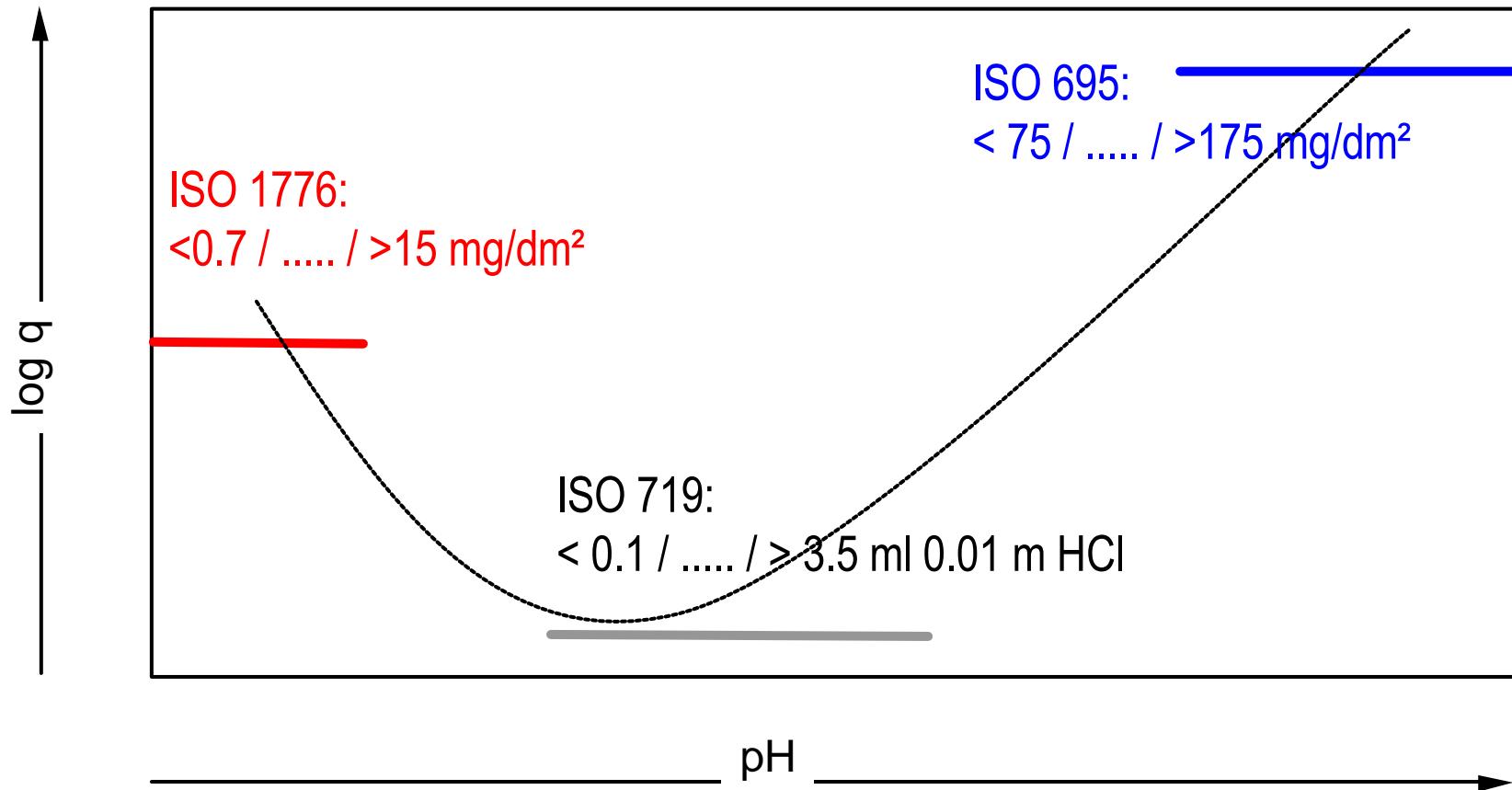


s or “SA/V” in cm^{-1}

dynamic tests

$$\dot{c} = q \cdot \dot{s}$$

designed for the family of conventional silicate glasses

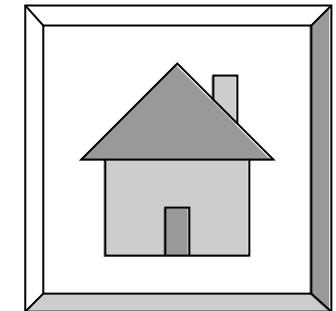


ISO standard tests:

ISO 1776 (stability against acidic attack)

area \approx 300 cm²; boil in 6 m HCl (1.5 l) for 6 h

$\Rightarrow <0.7 / 1.5 / 15 / >15$ mg/dm²



ISO 695 (stability against alkaline attack)

area 10=15 cm²; boil in 1 m NaOH + 1 m Na₂CO₃ (0.8 l) for 3 h ;

$\Rightarrow <75 / 175 / >175$ mg/dm²

ISO 719 (stability against hydrolytic attack)

powder 315-500 µm (4x 2 g); expose to 30 ml water in 50 ml flask

at 98 °C for 1 h; cool down; fill to 50 ml; titrate 25 ml aliquots by 0.01 m HCl

$\Rightarrow <0.1 / 0.2 / 0.85 / 2 / 3.5$ ml HCl per g glass

ISO 720 (stability against hydrothermal attack)

powder 300-420 µm (4x 10 g); expose to 50 ml water in 10 ml flask

at 121 °C for 0.5 h; cool down; fill to 10 ml; titrate by 0.02 m H₂SO₄

$\Rightarrow <0.1 / 0.85 / 1.5$ ml H₂SO₄ per g glass

*design of
glass corrosion experiments*

solution: *)

pH (free, buffered
compensated);
salts (e.g., 9 g/l NaCl);
organics;
redox (e.g., FeCl₂/FeCl₃)

temperature:

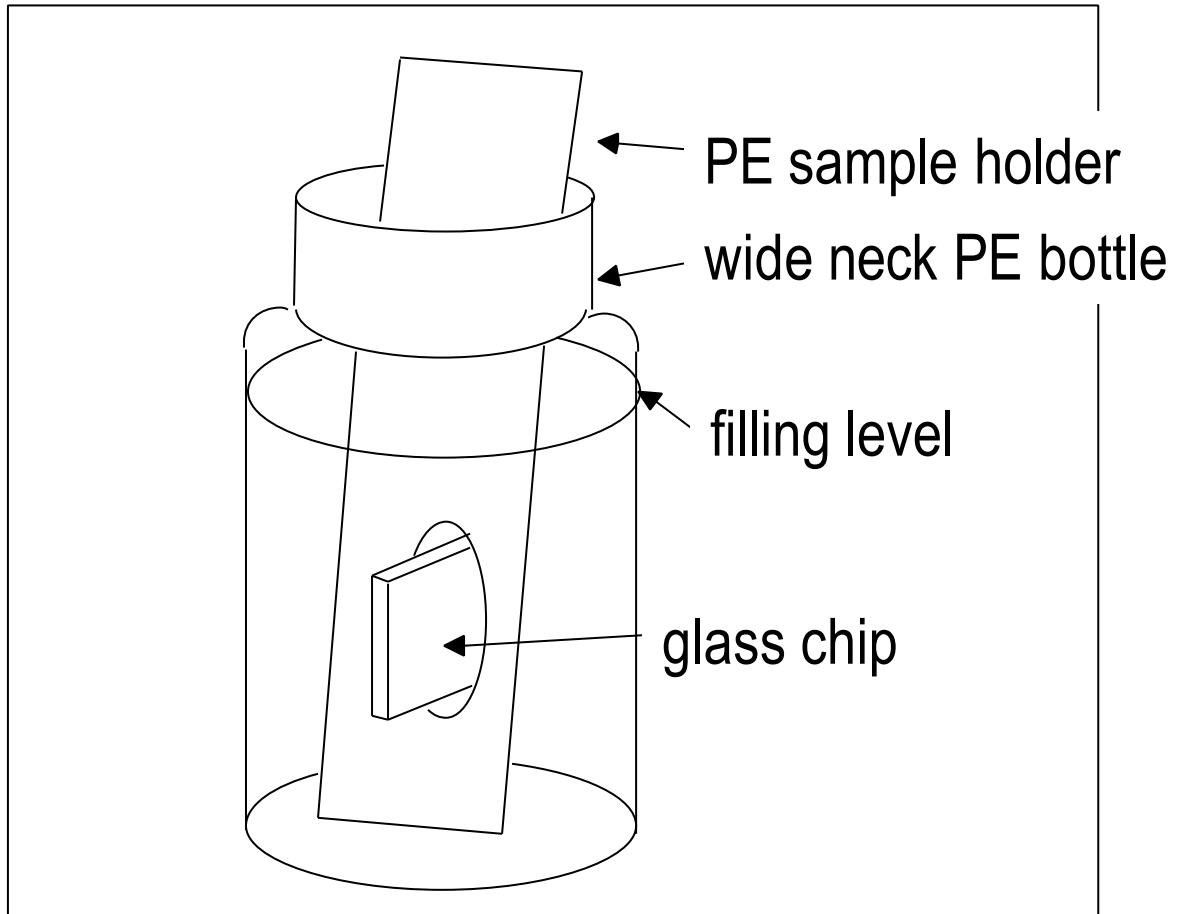
37±1 or 98±1 °C

s parameter:

0.1 cm⁻¹

time intervals:

0.5, 1, 2, 4, 8, 16 hours;
1, 3, 7, 14, 28, 60, 120, ... days



similar procedures: see MCC-1, MCC-2 tests

*) no „natural“ reference solution for corrosion experiments

solution: *)

pH (free, buffered
compensated);

salts (e.g., 9 g/l NaCl);

organics;

redox (e.g., $\text{FeCl}_2/\text{FeCl}_3$),

temperature:

37 ± 1 or 98 ± 1 °C

s parameter:

0.1 cm^{-1}

time intervals:

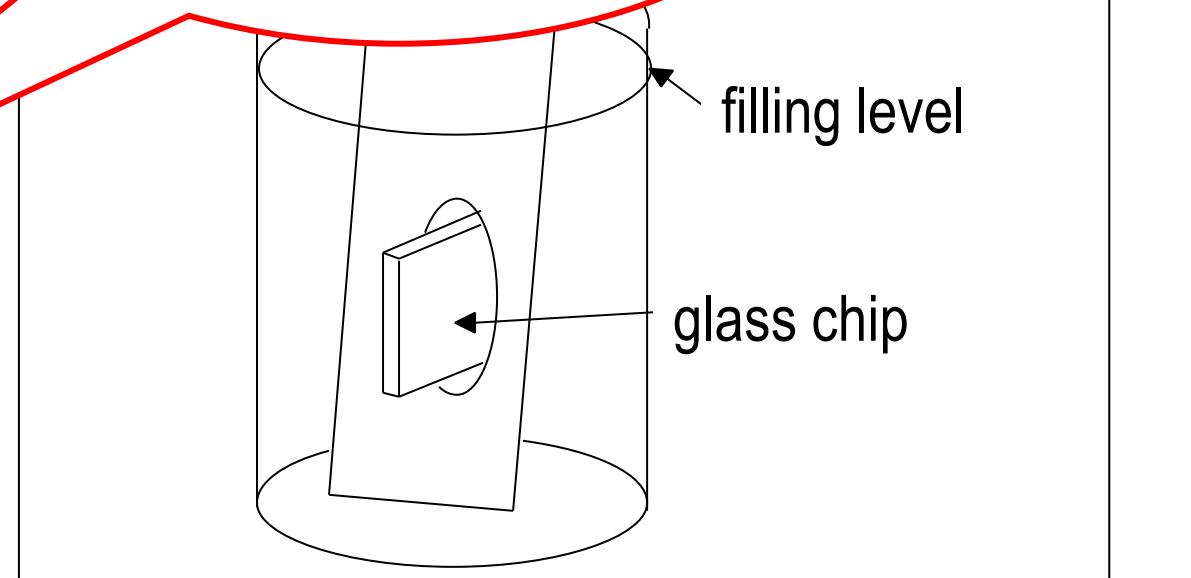
0.5, 1, 2, 4, 8, 16 hours;

1, 3, 7, 14, 28, 60, 120, ... days

$\pm 5 \text{ K}$ temperature error

make up for

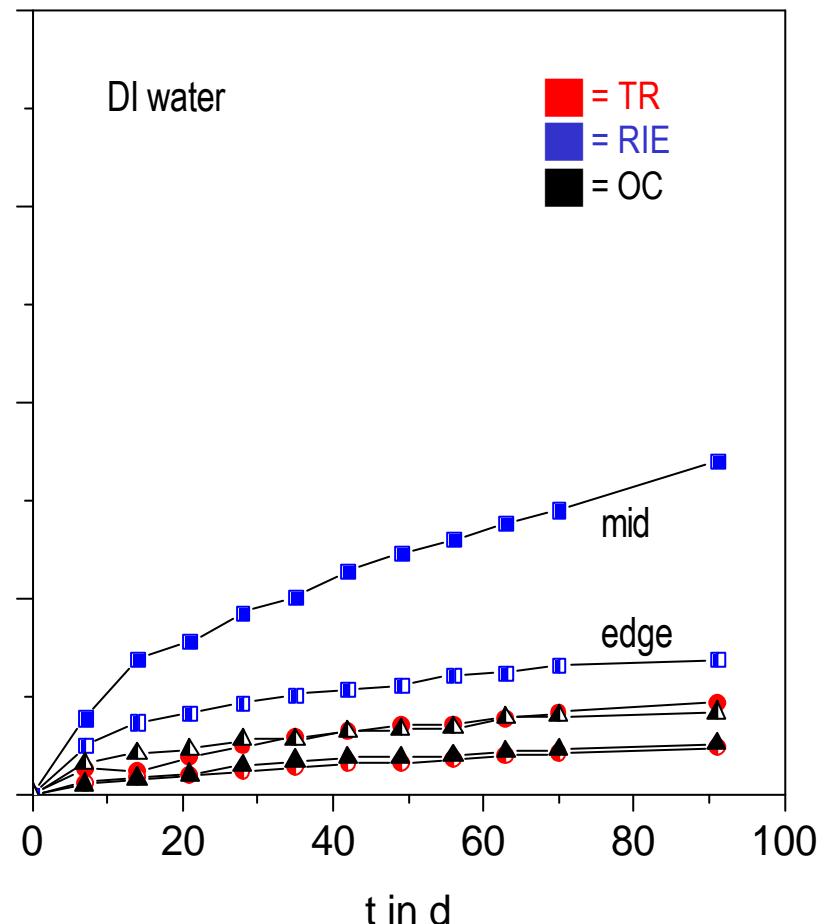
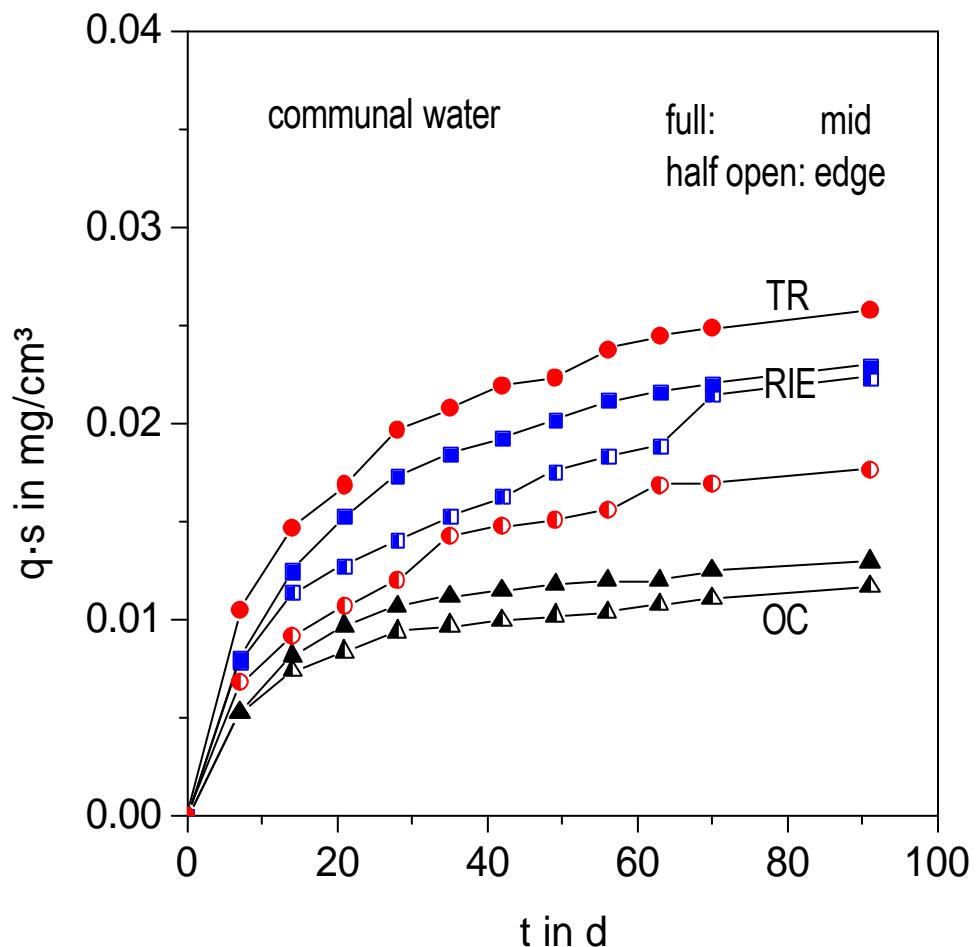
$\pm 40 \%$ error in mass loss

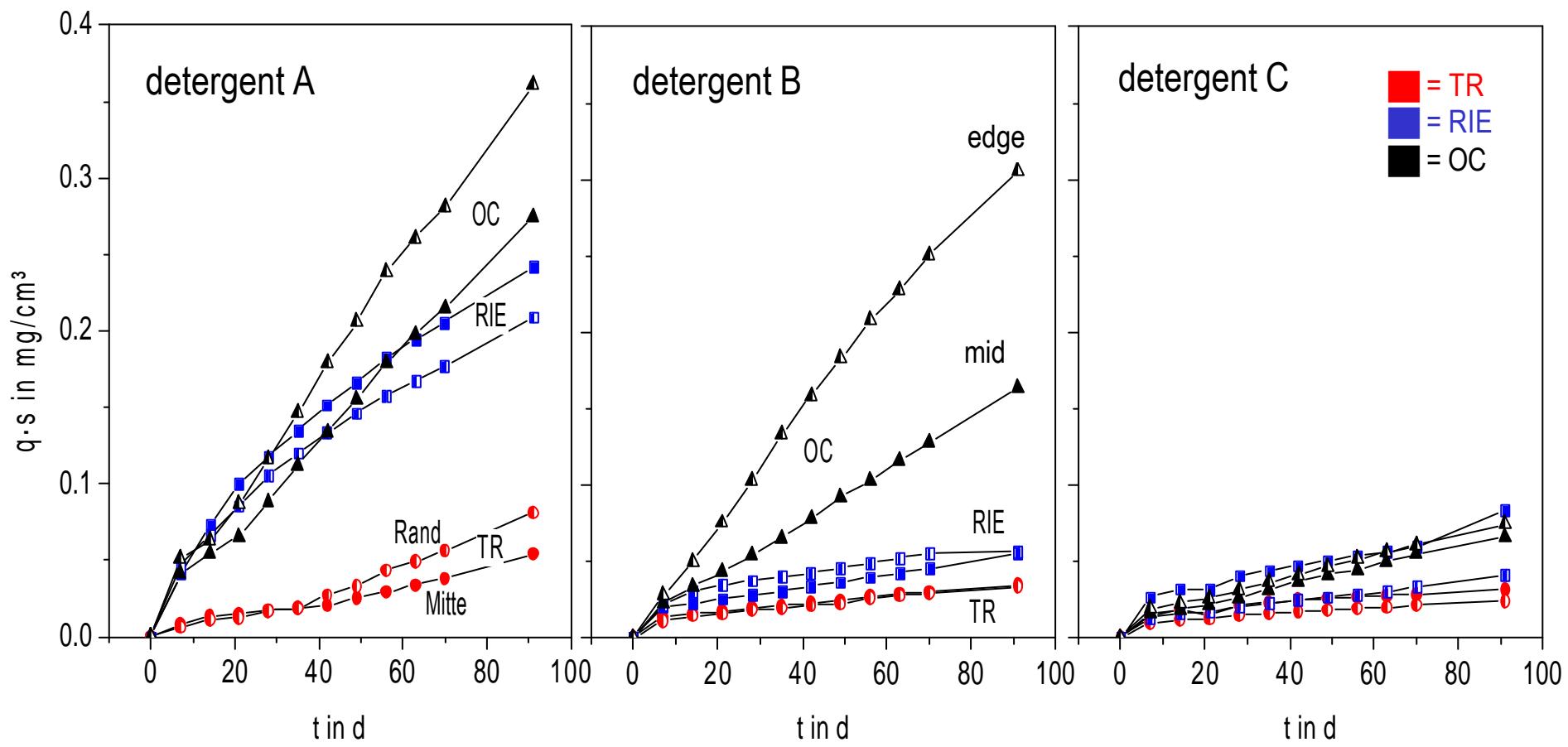


similar procedures: see MCC-1, MCC-2 tests

*) no „natural“ reference solution for corrosion experiments

	RIE	OC	TR
oxide composition			
SiO_2	60.20	72.50	69.30
ZrO_2	-	-	1.50
TiO_2	-	-	0.60
Al_2O_3	1.00	1.00	1.00
B_2O_3	0.70	-	-
MgO	-	4.11	-
CaO	-	7.10	4.90
ZnO	-	-	2.30
PbO	24.60	-	-
Na_2O	5.30	14.10	9.10
K_2O	8.70	-	10.00
sum	100.50	98.81	98.70
constitutional composition			
$2\text{ZnO}\cdot\text{SiO}_2$	-	-	3.16
$\text{ZrO}_2\cdot\text{SiO}_2$	-	-	0.90
$\text{CaO}\cdot\text{TiO}_2$	-	-	2.56
$\text{PbO}\cdot\text{SiO}_2$	31.35	-	-
$\text{K}_2\text{O}\cdot\text{Al}_2\text{O}_3\cdot 6\text{SiO}_2$	0.55	-	5.05
$\text{K}_2\text{O}\cdot 2\text{SiO}_2$	19.67	-	20.88
$\text{Na}_2\text{O}\cdot\text{Al}_2\text{O}_3\cdot 6\text{SiO}_2$	-	7.26	5.56
B_2O_3	0.70	-	-
$\text{MgO}\cdot\text{SiO}_2$	-	10.32	-
$\text{Na}_2\text{O}\cdot 2\text{SiO}_2$	15.64	31.50	20.72
$\text{Na}_2\text{O}\cdot 3\text{CaO}\cdot 6\text{SiO}_2$	-	25.13	13.55
SiO_2	32.10	25.80	27.63
sum	100.00	100.00	100.00



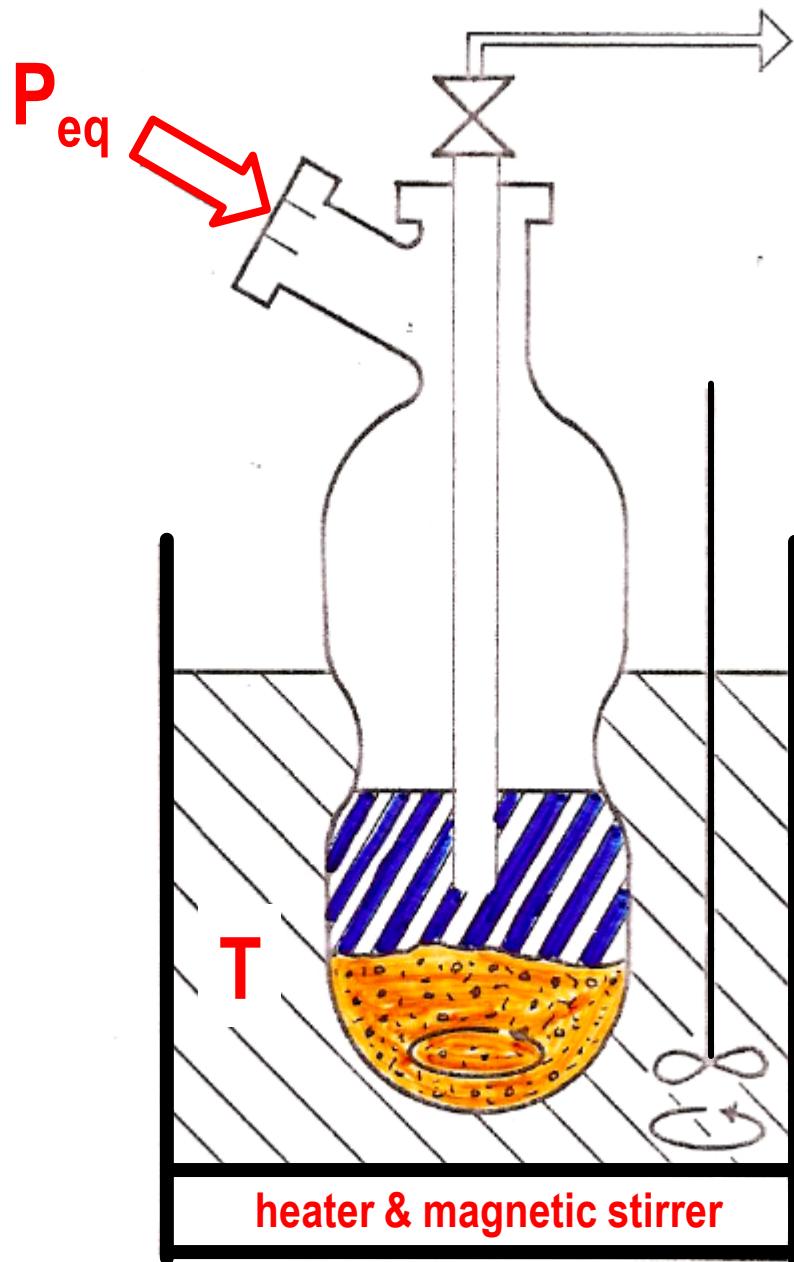


H_2O dest.
(specified by el. conductivity) → rapid change of pH takes place

buffered solutions → may interfere with the corrosion mechanism

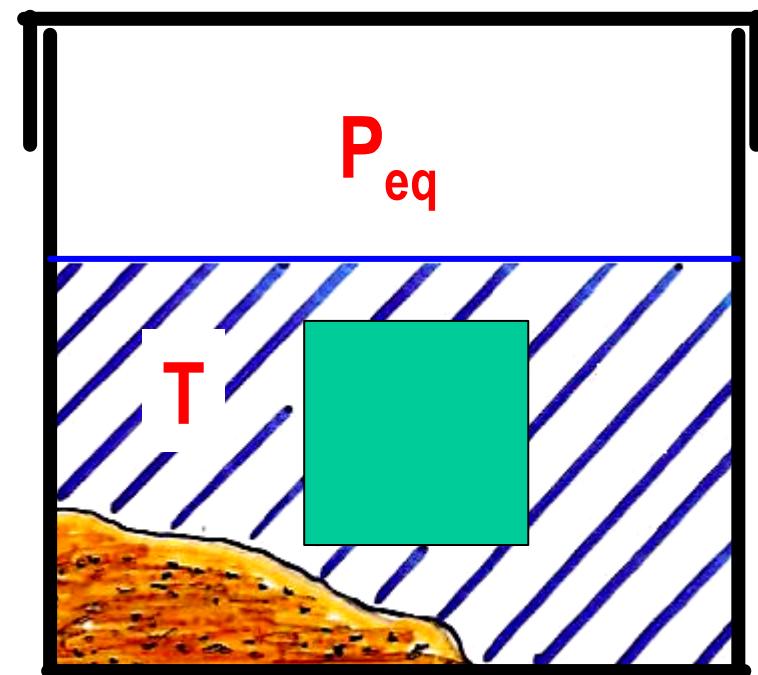
special corrosion media → for specific corrosion scenarios, e.g.,
- salt brines „Q“, „R“, ...;
- granitic or clay waters;
- simulated physiological fluids (9 g/l NaCl, Gamble's solution, ...)
- water with dish washing agents

water pre-saturated with glass powder



pre-saturation

example:
how to perform a corrosion test
under conditions „close to saturation“



corrosion test under saturation conditions

example: buffered solutions

citrate buffers

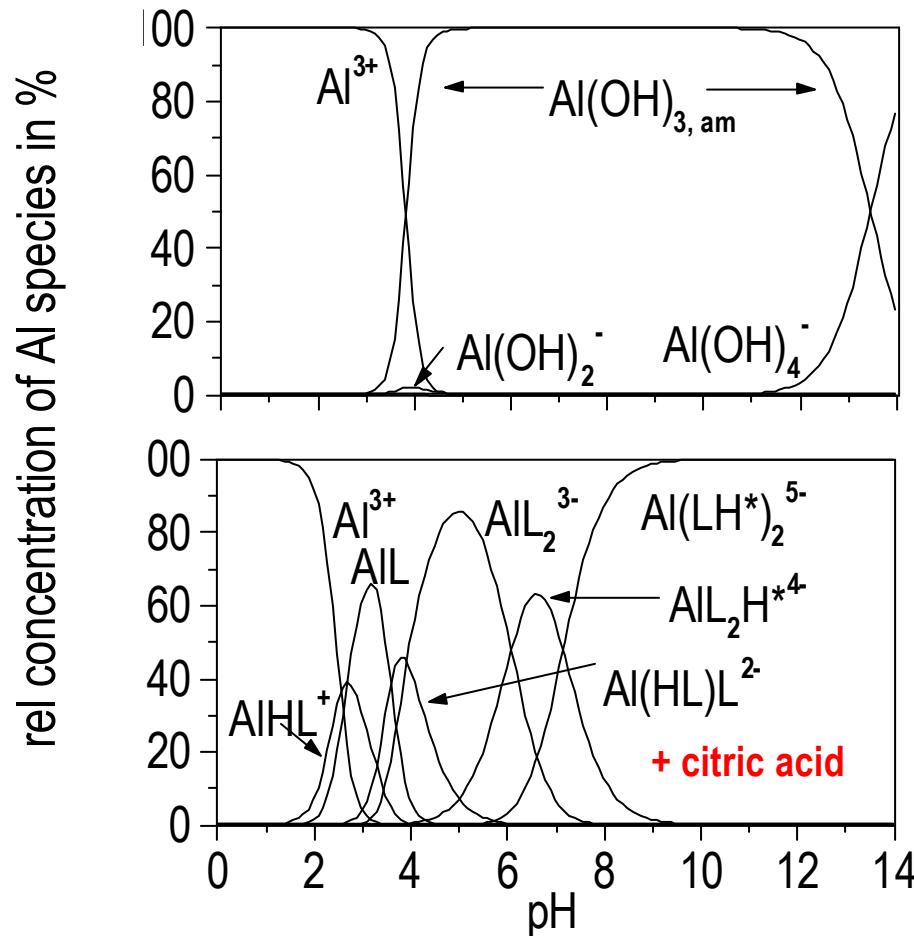
pH	C ₆ H ₈ O ₇ · H ₂ O [g]	NaCl [g]	Zusatz *) [ml]	
2	6.43	3.58	8.2	HCl
3	8.47	3.49	20.6	NaOH
4	11.75	2.57	68.0	NaOH
5	20.26	-	196.4	NaOH
6	12.53	-	159.6	NaOH

*) concentration 1 mol/l

Is a buffered constant pH solution
a good reference medium for corrosion tests?

NO WAY!

Citrate buffers, for example, destabilize the otherwise very stable alumina. Thus, very corrosion resistant glasses may appear to be very weak in a solution buffered with a citrate buffer.



surface pre-treatment:

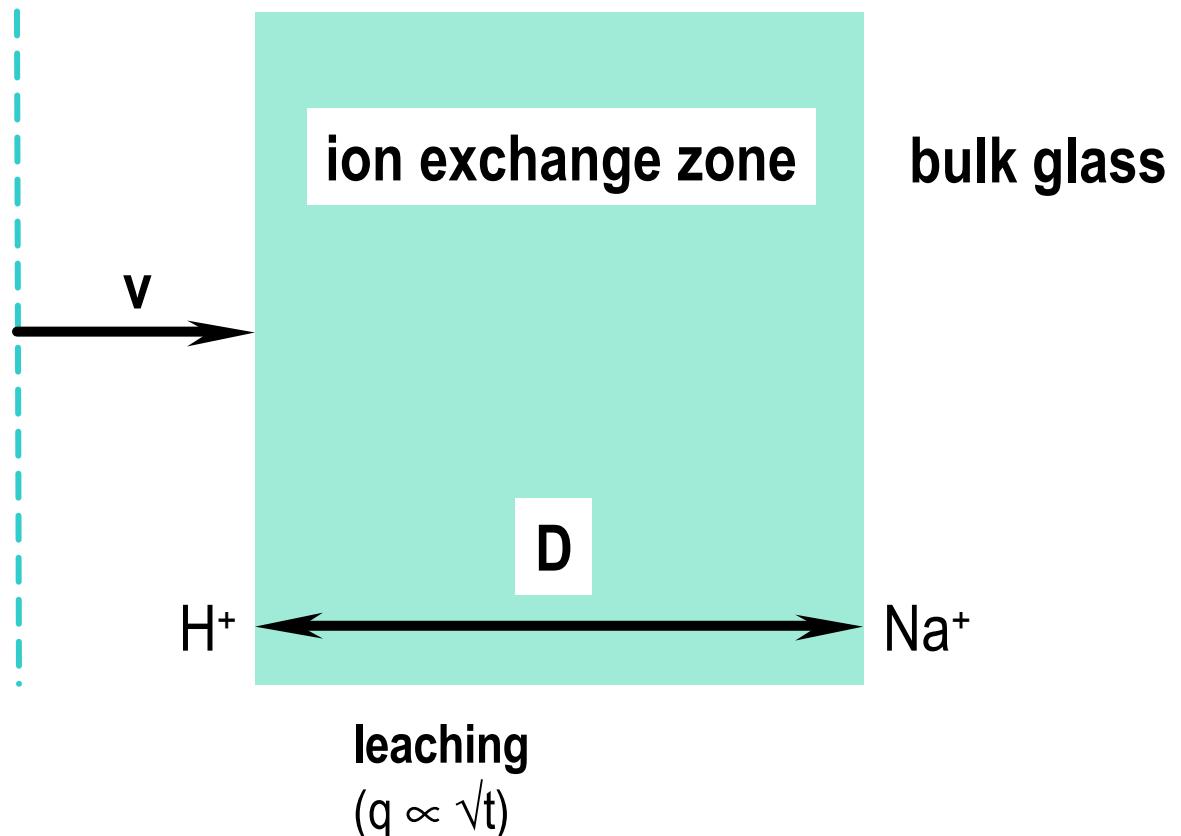
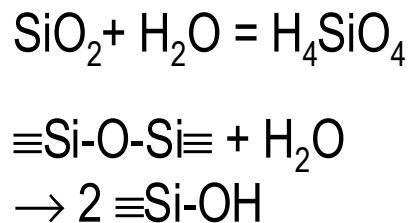
- cut by a low-speed saw in petroleum;
 - cut, ground, polished, etched in HF-HNO₃
 - as received from the production process
 - fire polished
 - blown glass foils
- etc. etc.

empirical knowledge

standard model

glass surface at t = 0

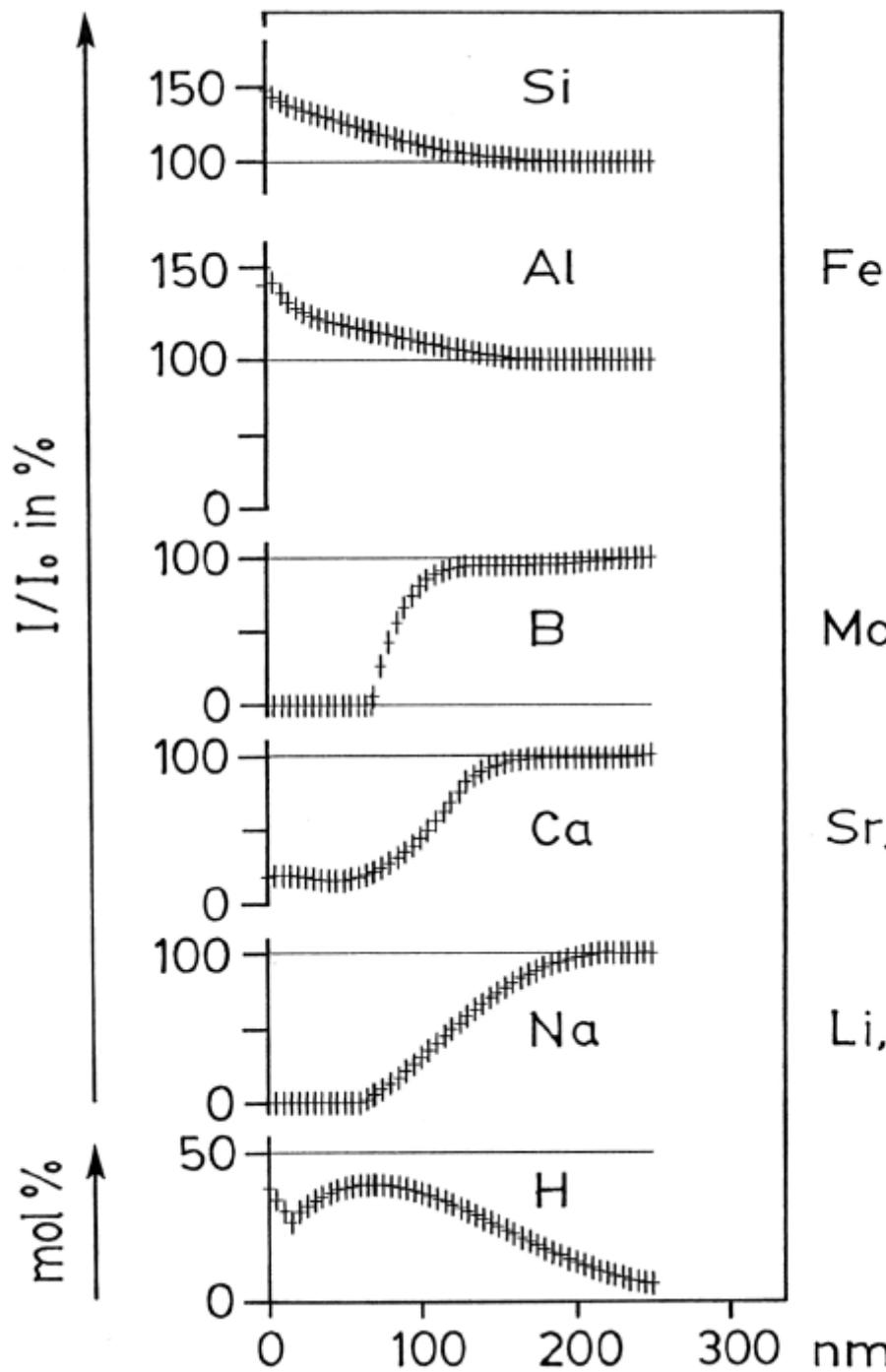
network dissolution
 $(q \propto t)$



The conclusion

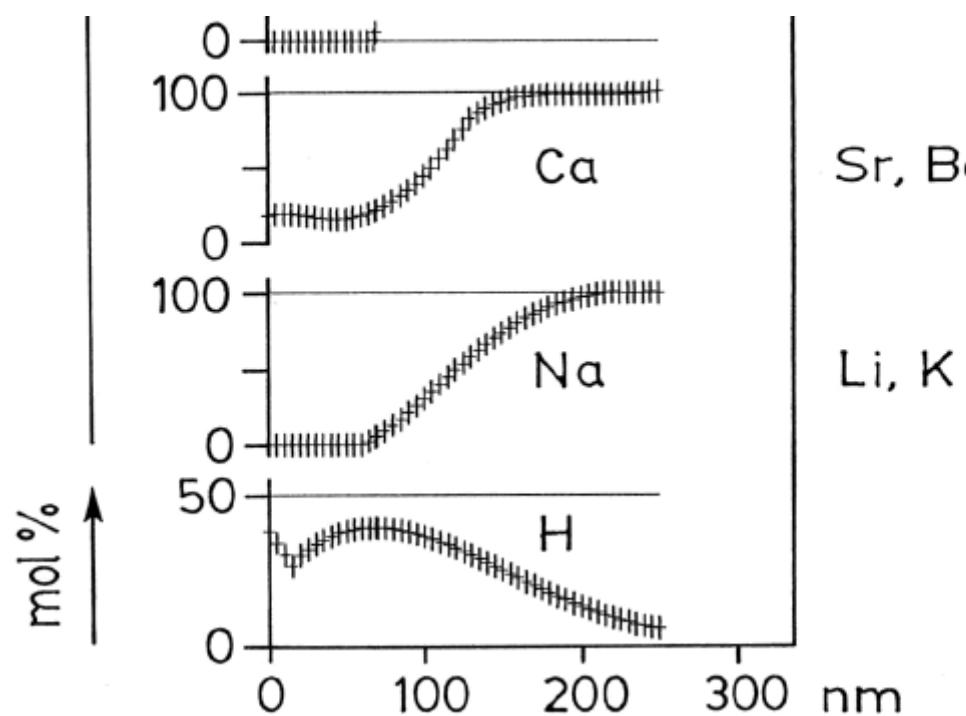
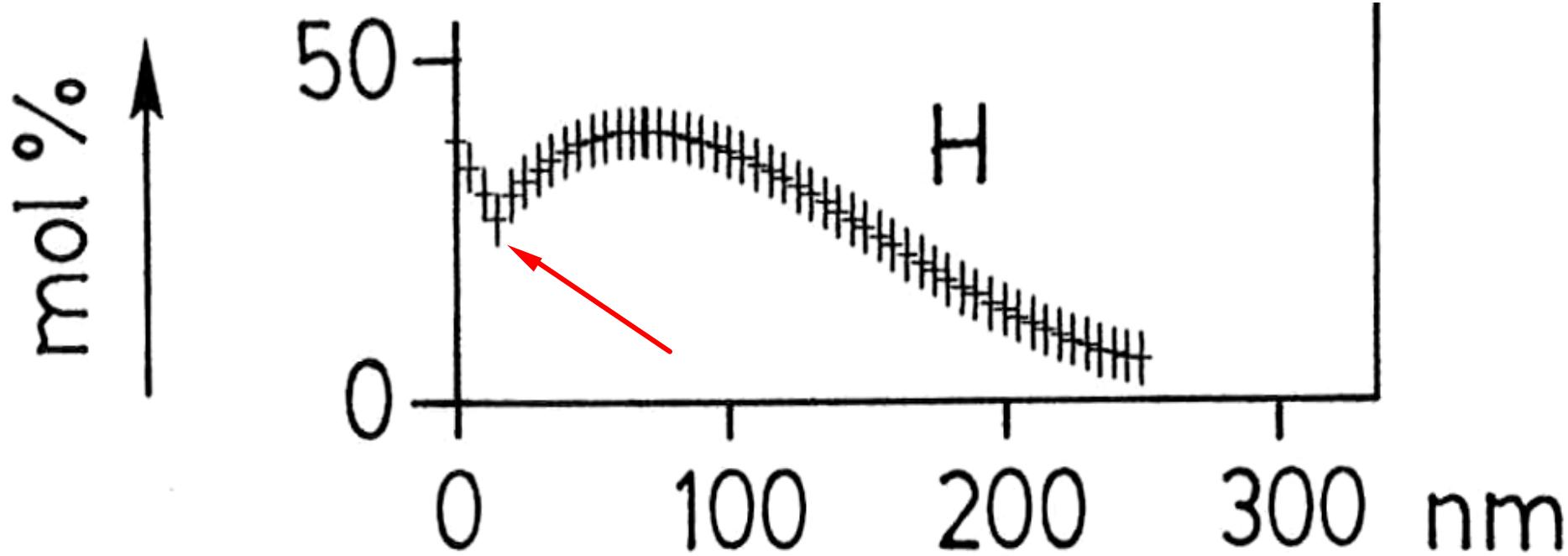
„the network modifiers are leached preferentially, the network formers are left behind as a scaffold dissolving slowly“ is misleading.

The covalent / ionic nature of the metal-oxygen bond has almost nothing to do with its stability against aqueous attack. Think of Si-O vs. P-O! Think of pure P_2O_5 vs. natural bones.
How would a $\text{MgO-B}_2\text{O}_3$ glass behave?

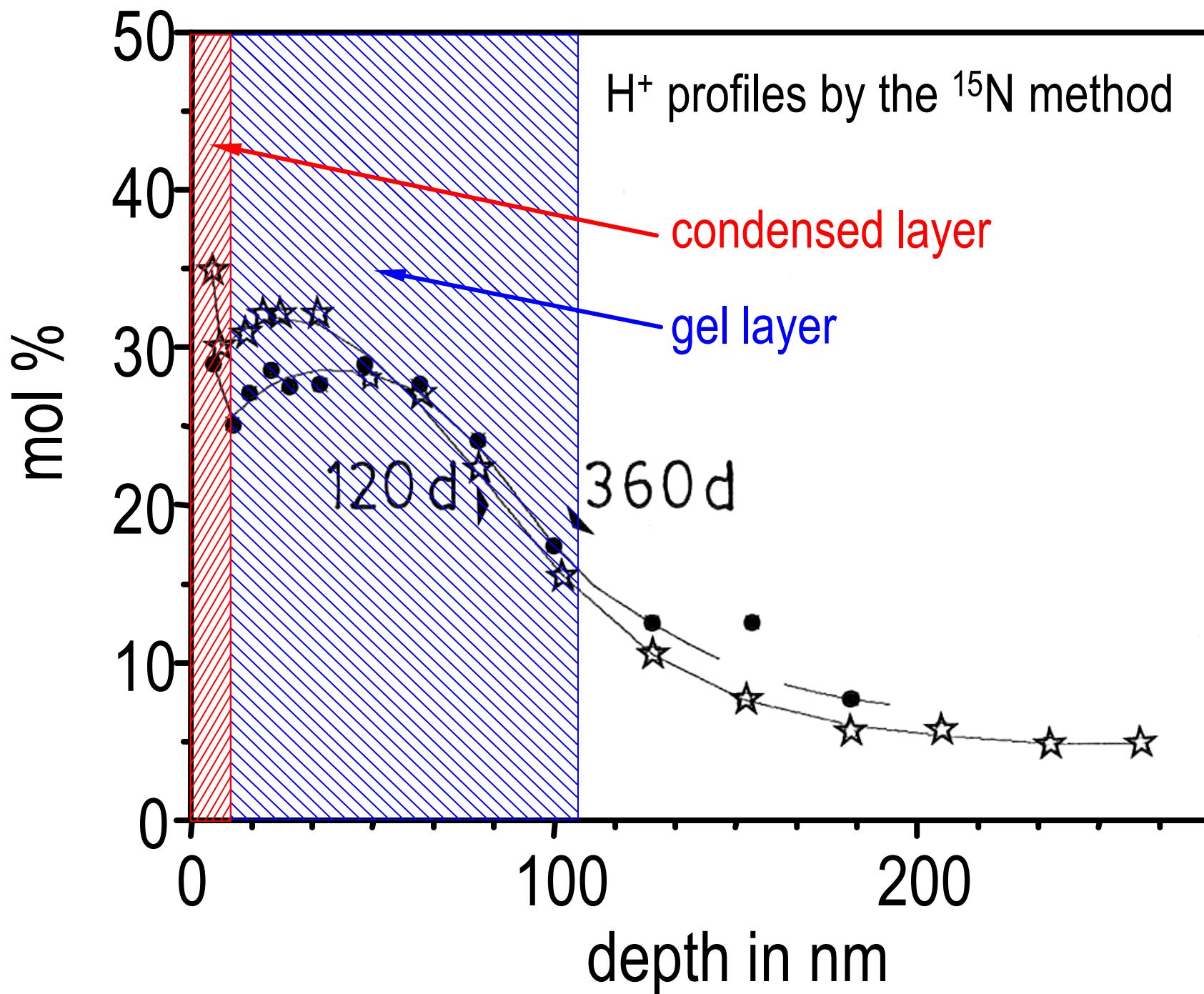


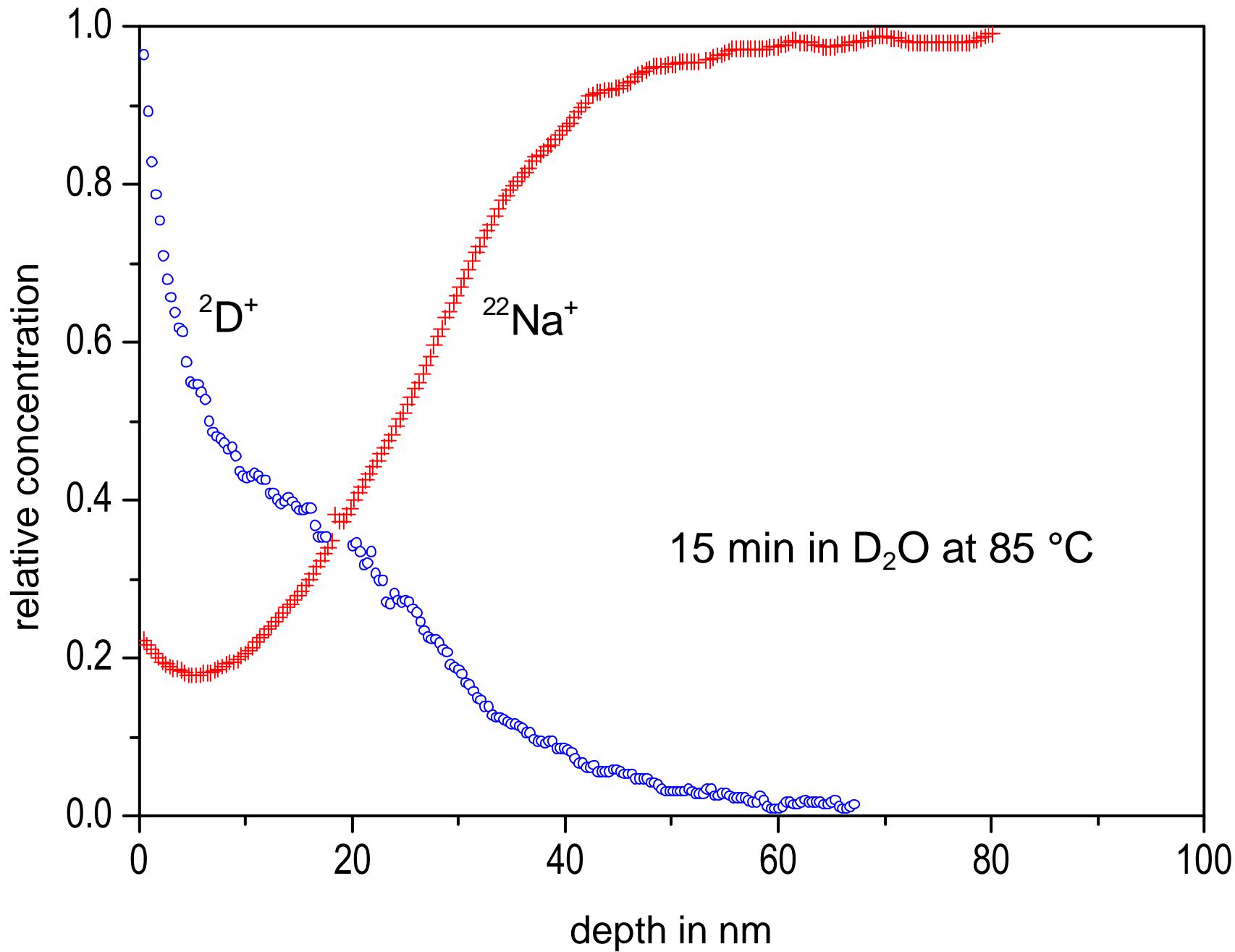
misleading view:
network modifiers are depleted,
network formers are enriched

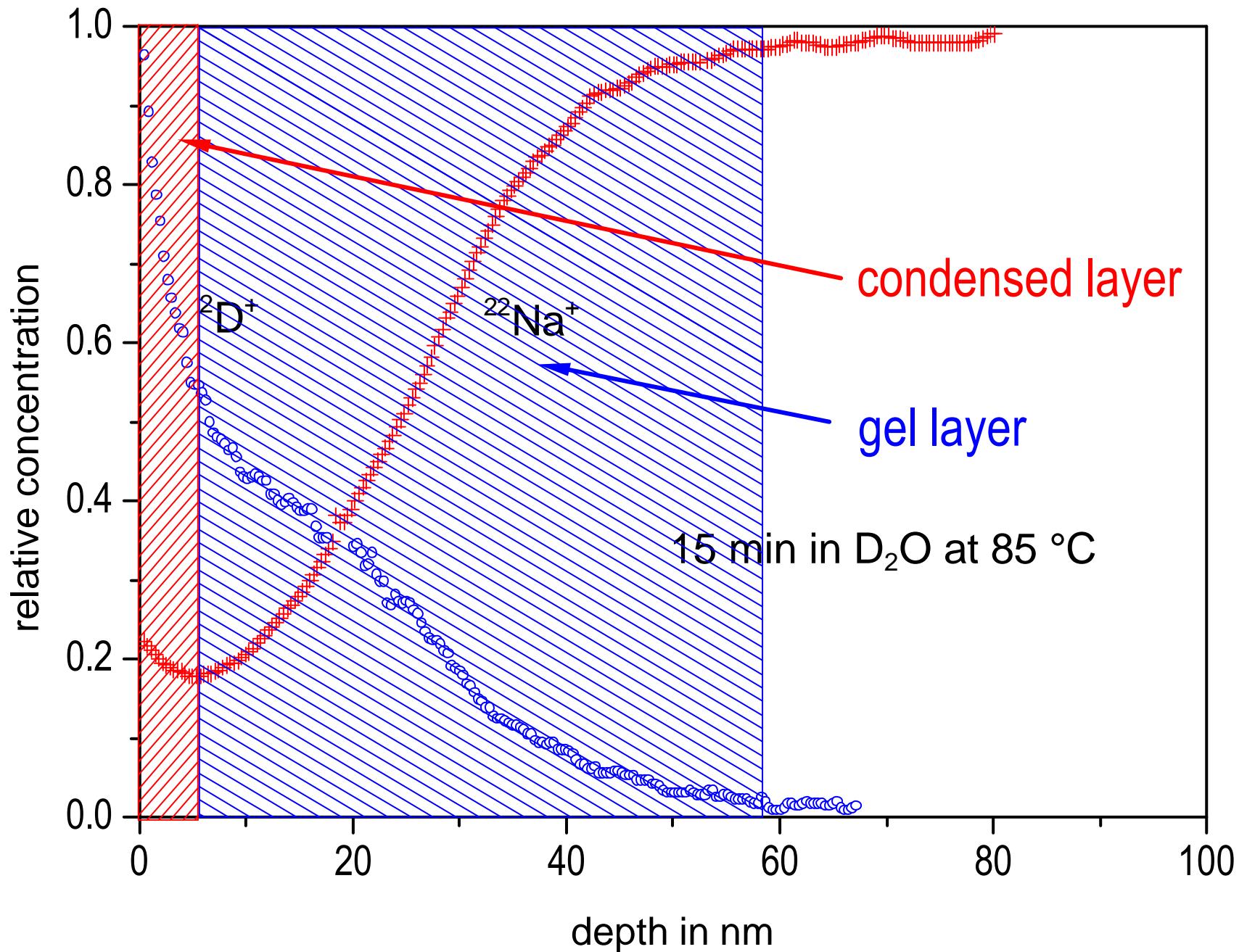
correct view:
an incongruent dissolution
process takes place;
the glass components are
enriched or depleted according
to their solubility in the aqueous
system

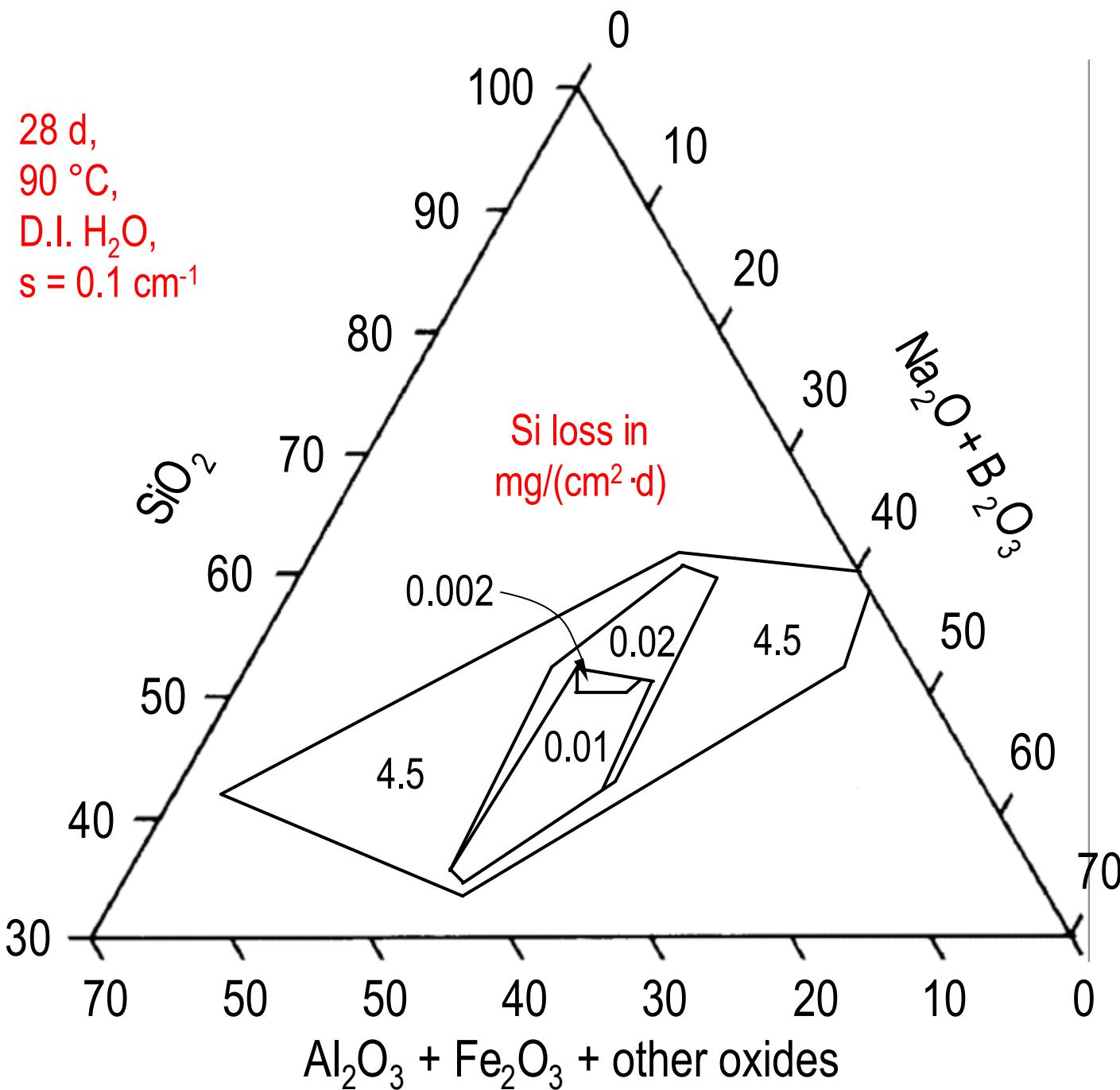


**new paradigm:
incongruent dissolution
according to the solubility
of individual oxides**









Let us learn from metallurgy:

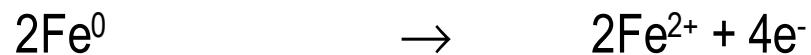
corrosion resistance =

f (thermodynamic stability, layer formation, passivation)

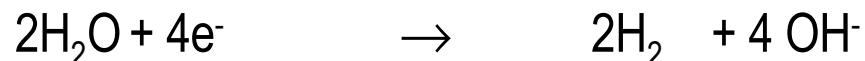
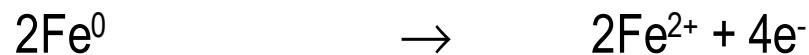
metals

the elementary process of metal corrosion is
electron transfer (redox reactions):

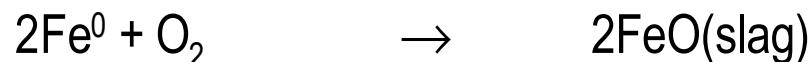
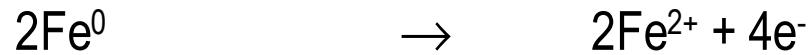
in air

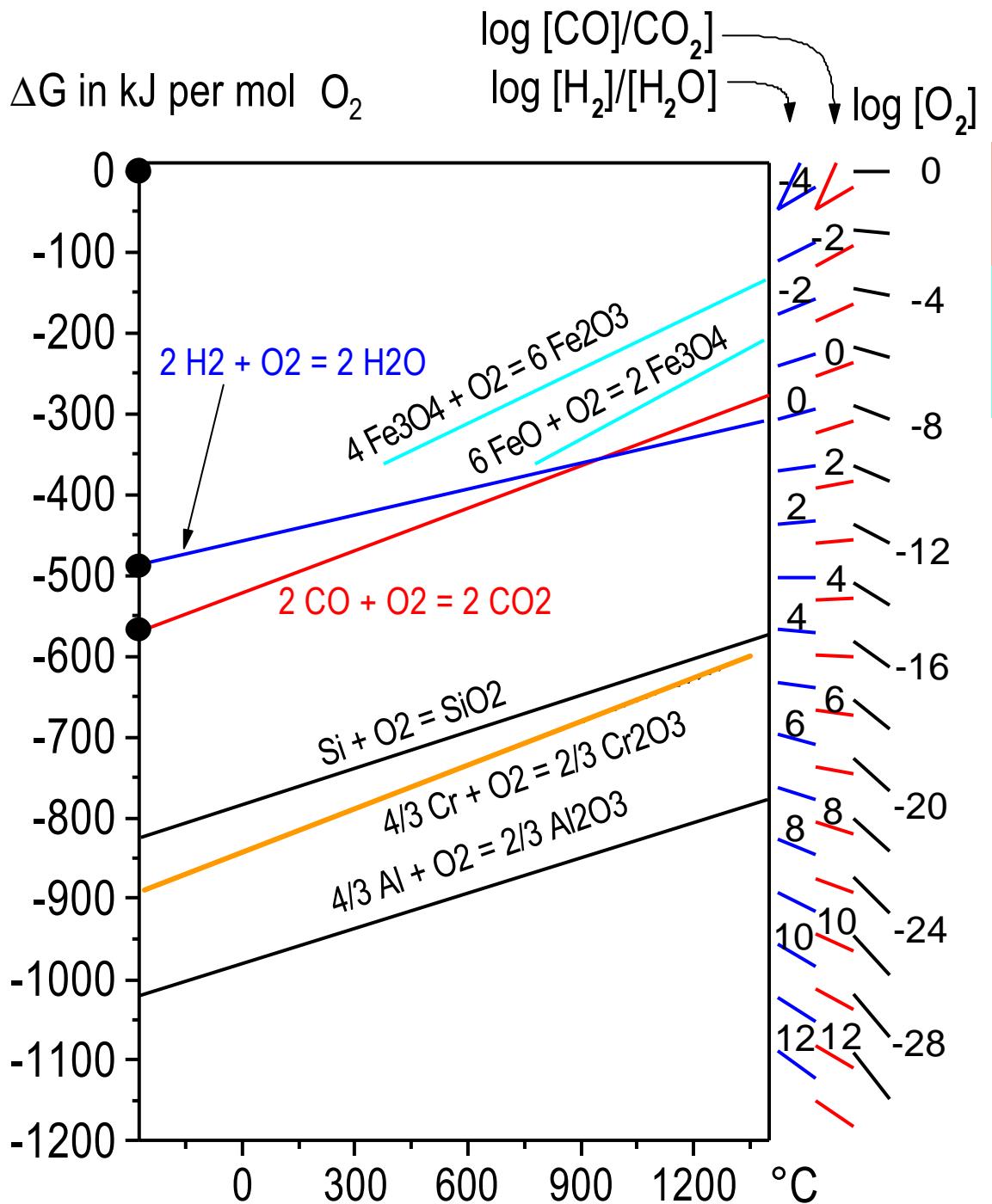


in water

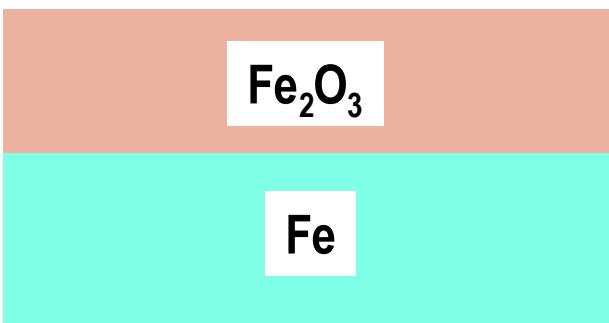


in a slag

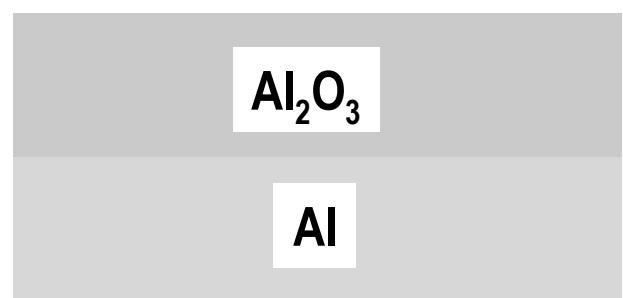




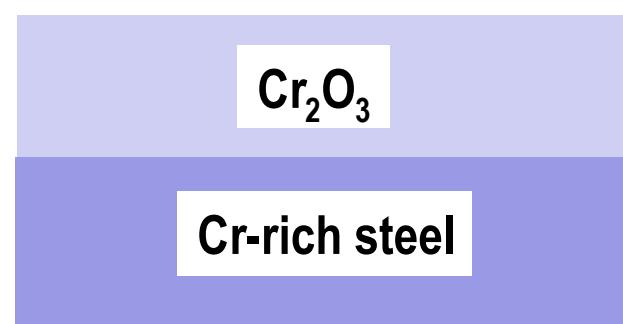
non-protective oxide scale:



protective oxide scale:

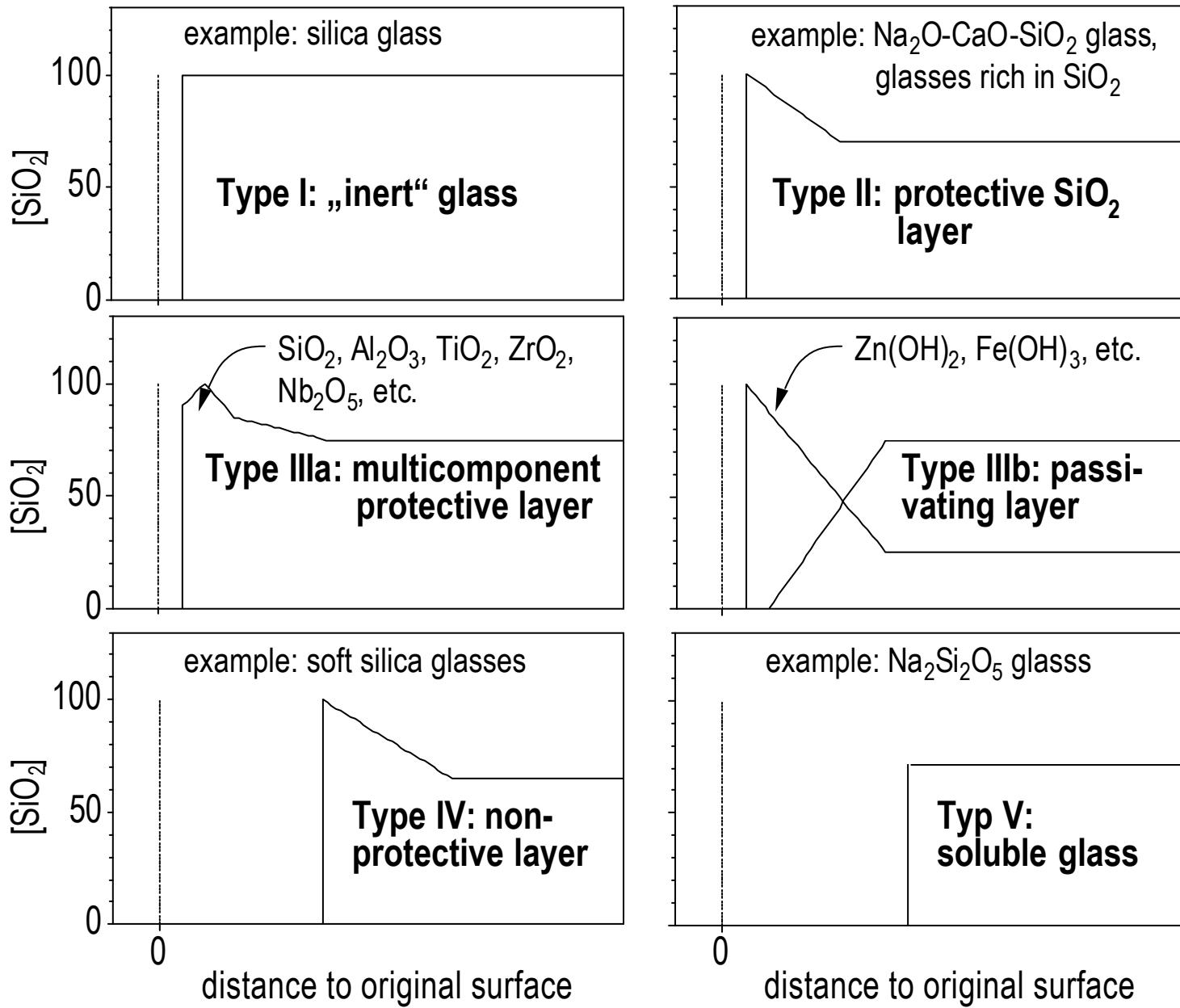


protective oxide scale:



The layer must

- be an effective diffusion barrier
- adhere well to the metal
- passivate the metal (forestall the e^- transfer)



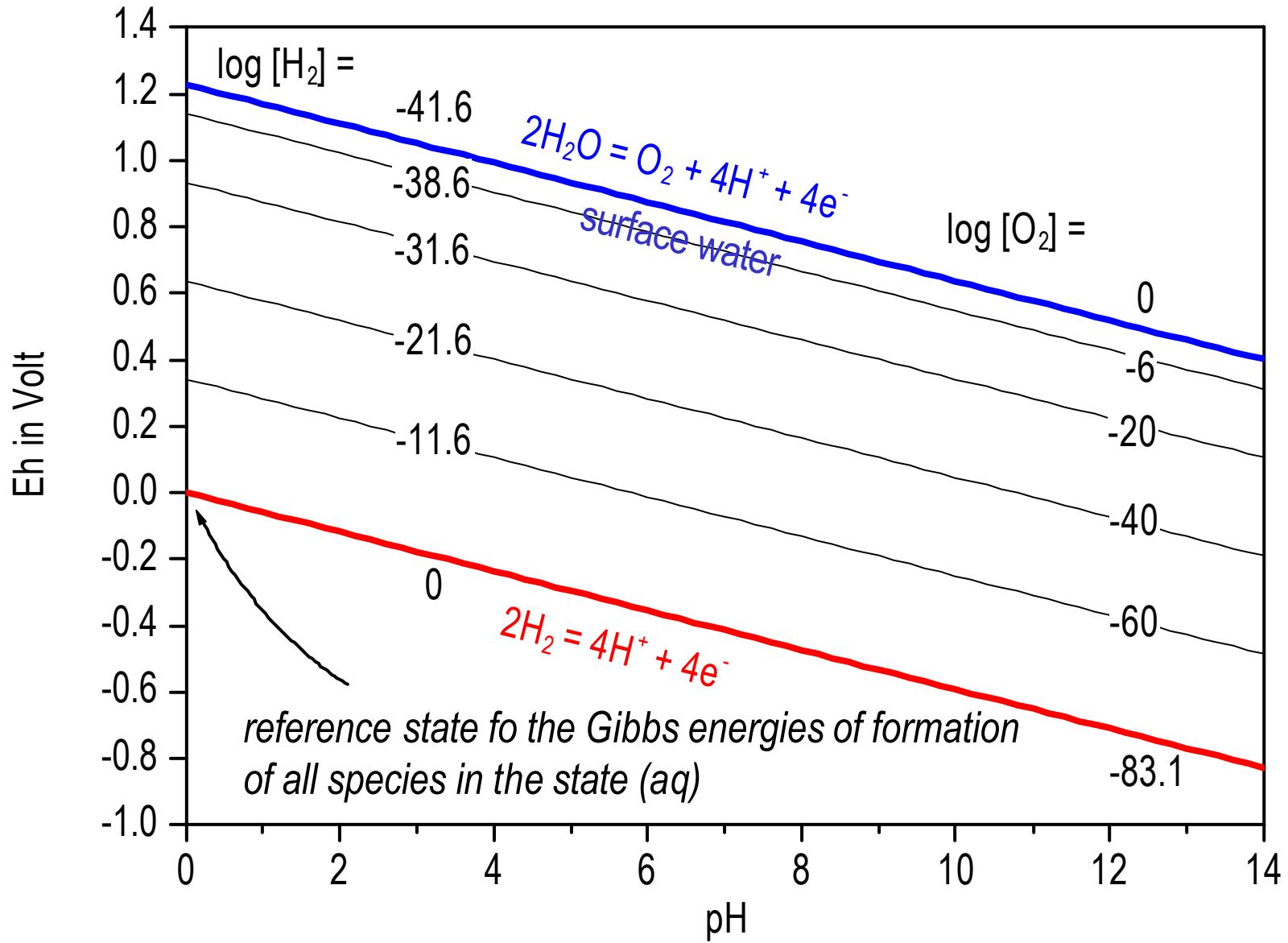
L.L. Hench

The layer must

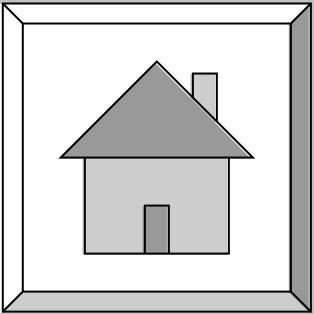
- be an effective diffusion barrier
- adhere well to the residual glass
- passivate the glass (forestall the H⁺ transfer)

the driving force of glass corrosion

$$2\text{H}_2\text{O} = 2\text{H}_2 + \text{O}_2; G_f^{\circ} = 474.360 \text{ kJ/mol}; K_f = 7.8 \cdot 10^{-84}$$

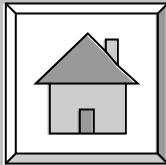


$$\text{H}_2\text{O} = \text{H}^+ + \text{OH}^-; G_w = 79.880 \text{ kJ/mol}; K_w = 1.0 \cdot 10^{-14}$$



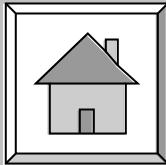
species	$-G_f^{\circ} \text{ (kJ/mol)}$
$\text{H}_2\text{O(l)}$	237.180
$\text{H}^+(\text{aq})$	0.000
$\text{H}_2\text{O} - \text{OH}^-(\text{aq}) = \text{H}^+(\text{aq})$	79.880
$\text{OH}^-(\text{aq})$	157.300
$\text{HO}_2^-(\text{aq})$	67.362
$\text{H}_2\text{O}_2(\text{l})$	134.097
$\text{H}_2(\text{aq})$	-17.573
$\text{O}_2(\text{aq})$	-16.318
$\text{H}_2(\text{g})$	0.000
$\text{O}_2(\text{g})$	0.000

The state „dissolved in water“ is a state like the states „solid“, „liquid“, and „gas“. It is denoted by (aq).



Spezies	-G ^f _e (kJ/mol)	Spezies	-G ^f _e (kJ/mol)
CO ₂ (g)	394.570	F ₂ (g)	0.000
CO ₂ (aq)	386.016	F ⁻	279.993
HCO ₃ ⁻	586.848	HF(aq)	298.110
CO ₃ ²⁻	527.895	HF ₂ ⁻	581.492
SiO ₂ (s)	854.910	P ₂ O ₅ (s)	1349.570
SiO ₂ (aq)	1307.760	H ₃ PO ₄ (aq)	1142.650
H ₃ SiO ₄ ⁻	1251.990	H ₂ PO ₄ ⁻	1130.391
H ₂ SiO ₄ ²⁻	1185.460	HPO ₄ ²⁻	1089.263
HSiO ₄ ³⁻	1116.547	PO ₄ ³⁻	1018.804
SiO ₄ ⁴⁻	1048.230	H ₄ P ₂ O ₇ (aq)	2032.160
H ₆ [H ₂ SiO ₄] ₄ ²⁻	5153.236	H ₃ P ₂ O ₇ ⁻	2026.830
H ₄ [H ₂ SiO ₄] ₄ ⁴⁻	5025.951	H ₂ P ₂ O ₇ ²⁻	2003.410
HSiO ₃ ⁻	1005.46	HP ₂ O ₇ ³⁻	1961.710
SiO ₃ ²⁻	938.51	P ₂ O ₇ ⁴⁻	1919.200
		H ₅ P ₃ O ₁₀ (aq)	2921.670
Al ₂ O ₃ (s)	1583.150	H ₄ P ₃ O ₁₀ ⁻	2923.190
Al ³⁺	492.000	H ₃ P ₃ O ₁₀ ²⁻	2917.480
Al(OH) ²⁺	700.653	H ₂ P ₃ O ₁₀ ³⁻	2094.550
Al(OH) ₂ ⁺	907.384	HP ₃ O ₁₀ ⁴⁻	2872.550
Al(OH) ₃ (aq)	1111.061	P ₃ O ₁₀ ⁵⁻	2821.490
Al(OH) ₃ (am)	1137.630		
Al(OH) ₄ ⁻	1305.410	B ₂ O ₃	1194.270
		H ₃ BO ₃ (aq)	968.638
Fe ₂ O ₃ (s)	739.960	H ₂ BO ₃ ⁻	917.564
Fe ³⁺	17.866	HBO ₃ ²⁻	845.695
FeOH ²⁺	240.413	BO ₃ ³⁻	769.182
Fe(OH) ₂ ⁺	457.228		
Fe(OH) ₃ (aq)	670.695	TiO ₂	889.940
Fe(OH) ₃ (s)	696.636	TiO ²⁺	577.392
Fe(OH) ₄ ⁻	841.821	TiO ₂ OH ⁻	467.353
		TiO(OH) ₂ s	1058.552
FeO	250.990		
Fe ²⁺	92.257	ZrO ₂	1036.870
FeOH ⁺	279.951	Zr ⁴⁺	594.128
Fe(OH) ₂ (aq)	457.102	ZrO ²⁺	843.076
Fe(OH) ₂ (s)	486.599	ZrO ₂ OH ⁻	1203.737
Fe(OH) ₃ ⁻	619.232	ZrO(OH) ₂ s	1303.316

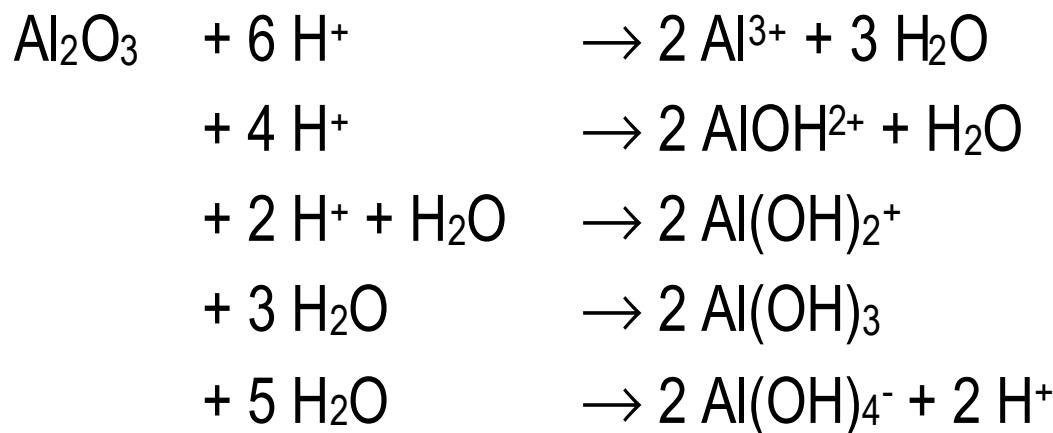
Spezies	-G ^f _e (kJ/mol)	Spezies	-G ^f _e (kJ/mol)
MgO(s)	569.840	PbO(s)	188.489
Mg ²⁺	455.261	Pb ²⁺	24.393
MgOH ⁺	638.064	PbOH ⁺	226.354
Mg(OH) ₂ (aq)	769.438	Pb(OH) ₂ (aq)	400.827
Mg(OH) ₂ (s)	833.746	Pb(OH) ₃ ⁻	575.718
MgCO ₃ (aq)	1002.486		
MgCO ₃ (s)	1012.110	BaO(s)	528.690
MgHCO ₃ ⁻	1050.602	Ba ²⁺	547.518
CaO(s)	604.460	Li ₂ O(s)	561.760
Ca ²⁺	552.706	Li ⁺	292.629
CaOH ⁺	716.970		
Ca(OH) ₂ (aq)	868.138	Na ₂ O(s)	376.740
Ca(OH) ₂ (s)	897.008	Na ⁺	262.211
CaCO ₃ (aq)	1081.438		
CaCO ₃ (s)	1128.760	K ₂ O(s)	322.200
CaHCO ₃ ⁻	1145.035	K ⁺	282.671
SrO(s)	562.680	Cs ₂ O(s)	308.300
Sr ²⁺	571.451	Cs ⁺	292.001
SrOH ⁺	733.455		
Sr(OH) ₂ (aq)	871.109	Nd ₂ O ₃ (s)	1721.700
Sr(OH) ₂ (s)	881.987	Nd ³⁺	671.532
SrCO ₂ (aq)	1087.338	Nd ₂ (OH) ₂ ⁴⁺	1738.230
SrCO ₃ (s)	1140.140	Nd(OH) ²⁺	863.126
		Nd(OH) ₃ (s)	1259.221
MnO(s)	363.340	Nd(OH) ₄ ⁻	1407.096
Mn ²⁺	229.953		
MnOH ⁺	406.685	MoO ₃ (s)	655.778
Mn(OH) ₂ (s)	615.048	MoO ₂ ²⁺	411.287
Mn(OH) ₃ ⁻	746.426	MoO ₂ (OH) ⁺	645.884
		H ₂ MoO ₄ (aq)	877.134
ZnO(s)	318.470	HMnO ₄ ⁻	866.632
Zn ²⁺	147.193	MoO ₄ ²⁻	838.055
ZnOH ⁺	333.256		
Zn(OH) ₂ (aq)	535.385	Nb ₂ O ₅ (s)	1765.82
Zn(OH) ₃ ⁻	704.711	Nb(OH) ₅ (aq)	1448.50
Zn(OH) ₄ ²⁻	871.276	NbO ₃ ⁻	932.20

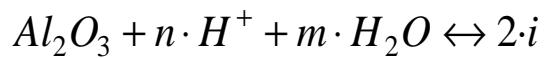


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Zn(OH) ₄ ²⁻	871.276	NbO ₃ ⁻	932.20

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Al^{3+}	492.000
Al(OH)^{2+}	700.653
Al(OH)_2^+	907.384
$\text{Al(OH)}_3(\text{aq})$	1111.061
$\text{Al(OH)}_3(\text{am})$	1137.630
Al(OH)_4^-	1305.410





$$K_i = \frac{a_i^2}{[Al_2O_3] \cdot [H^+]^n \cdot [H_2O]^m}$$

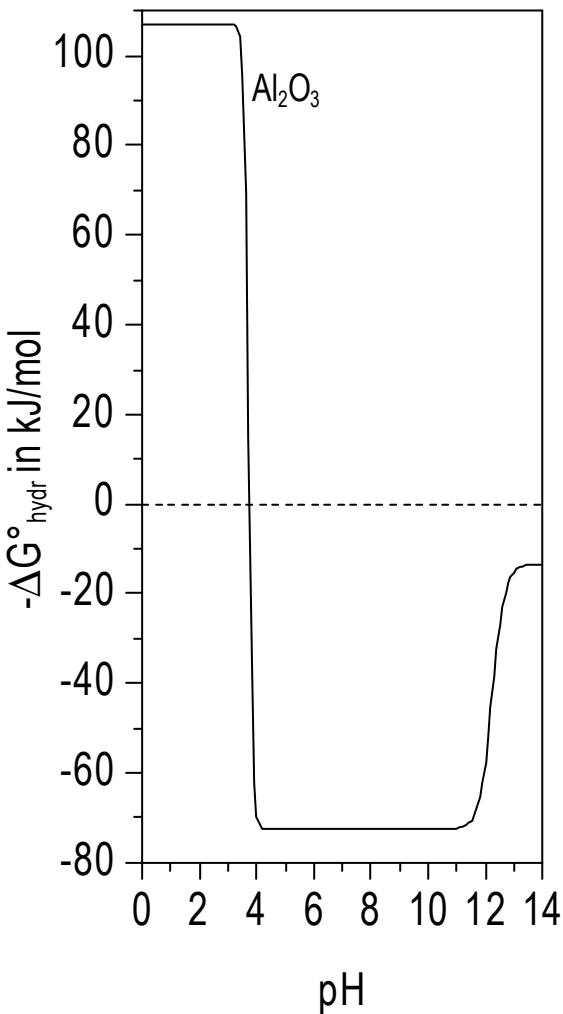
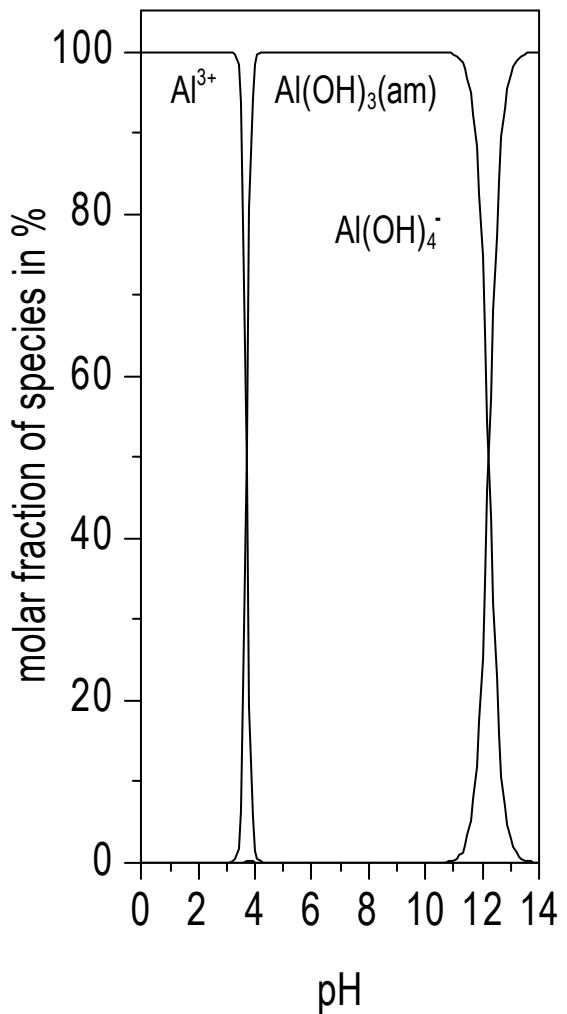
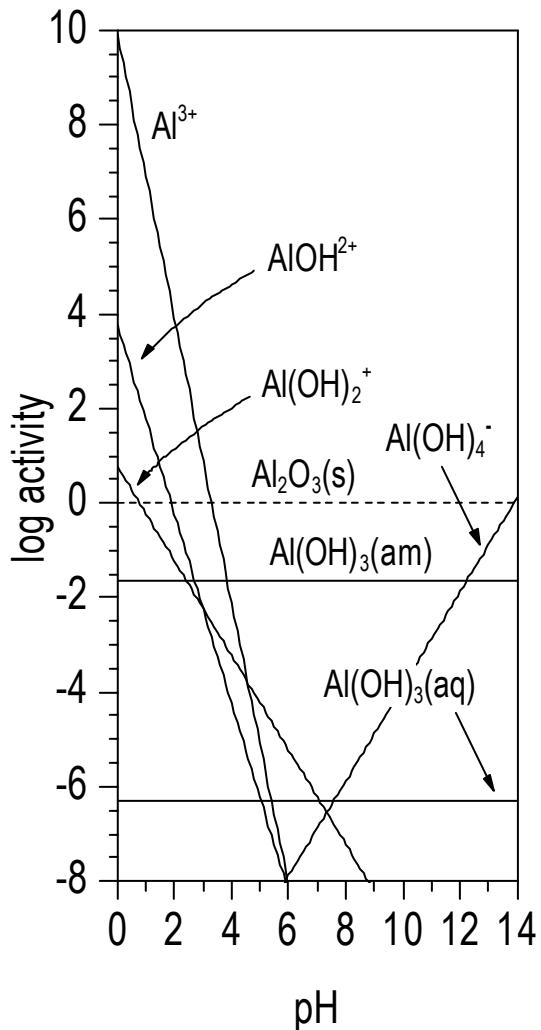
$$\log a_i = \frac{1}{2} \cdot \log K_i - \frac{n}{2} \cdot pH$$

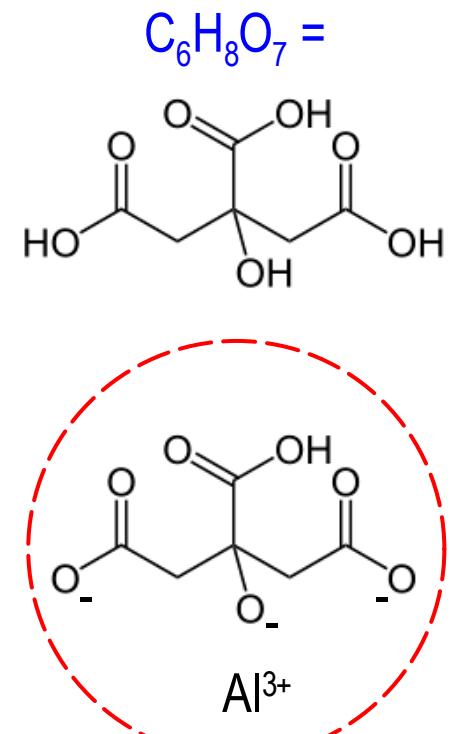
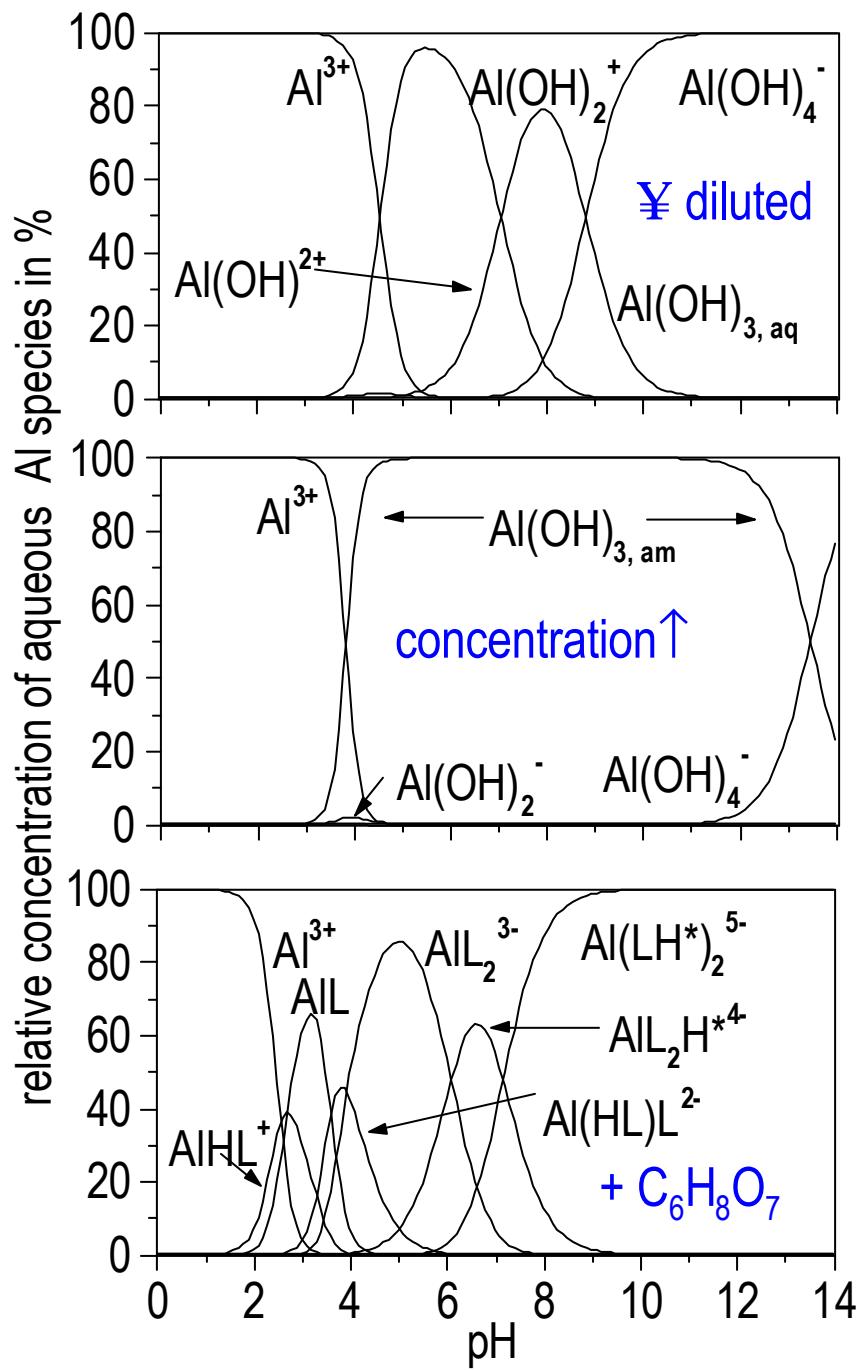
$$x_i = \frac{10^{\log a_i}}{\sum 10^{\log a_i}}$$

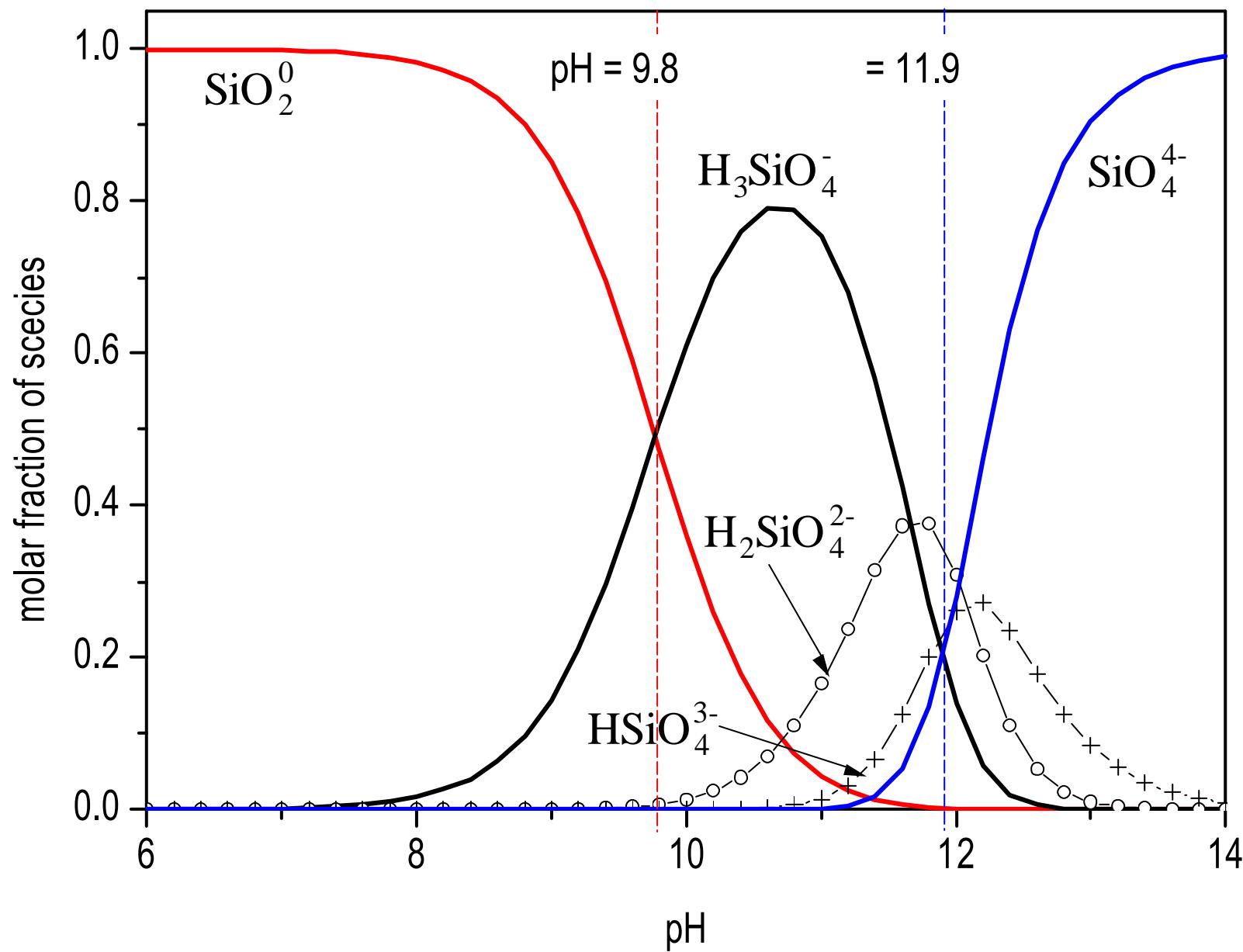
$$species \% = 100 \cdot x_i$$

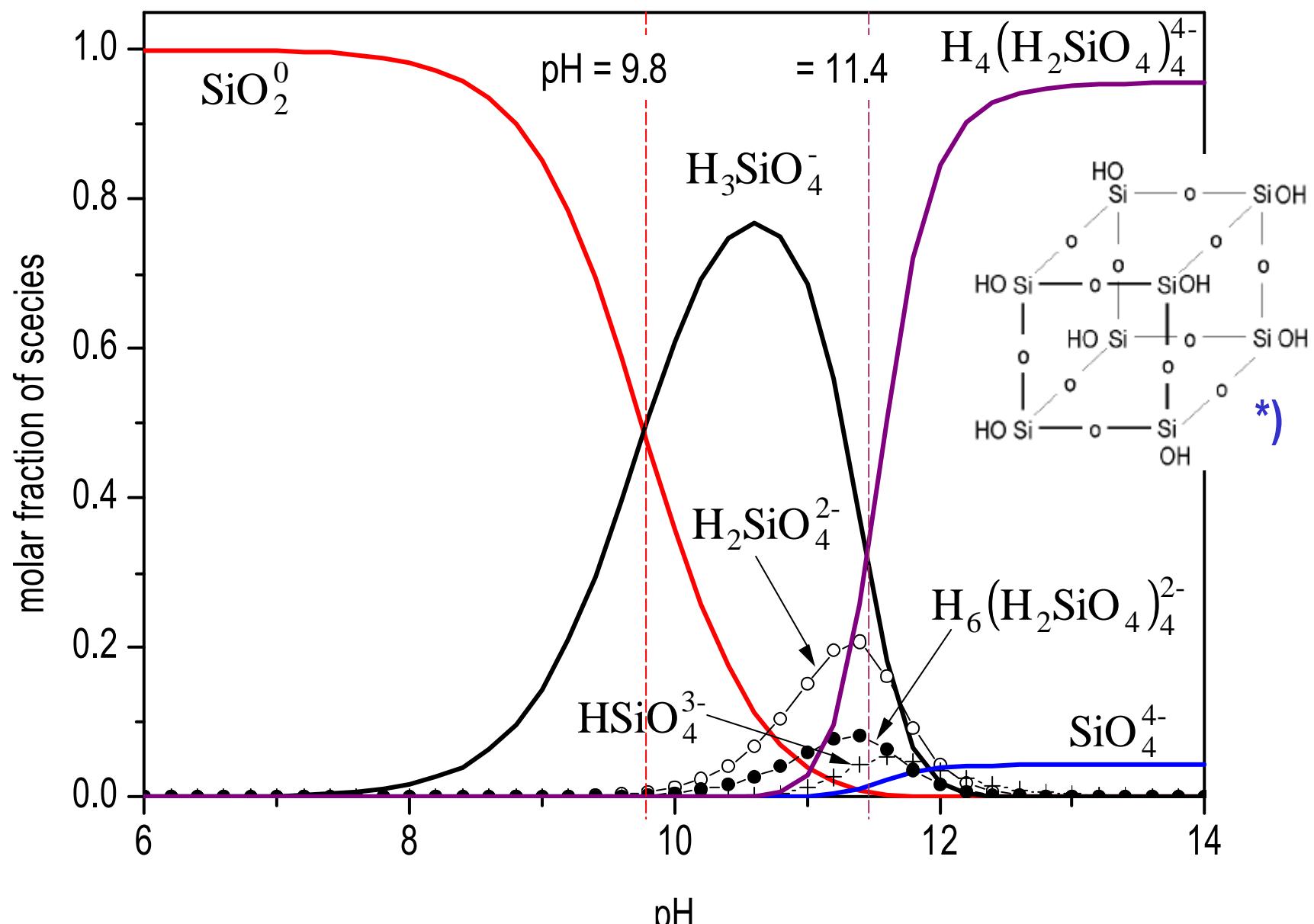
$$-\Delta G_{hydr}^o(Al_2O_3) =$$

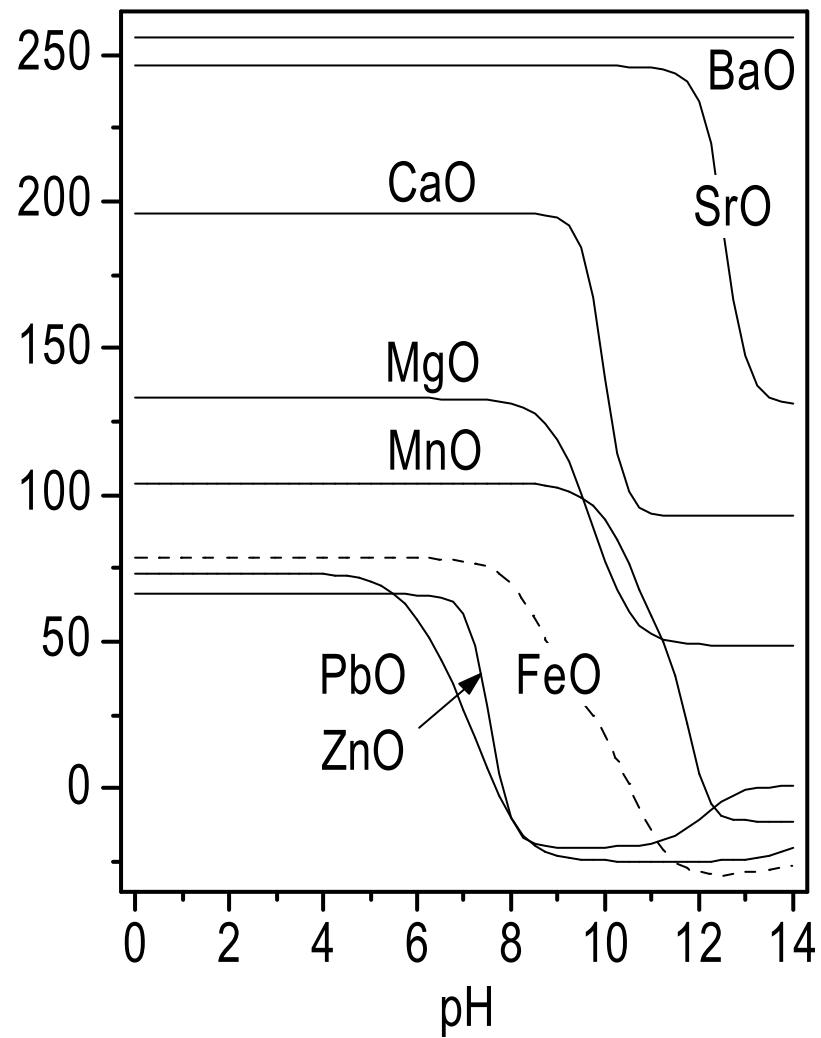
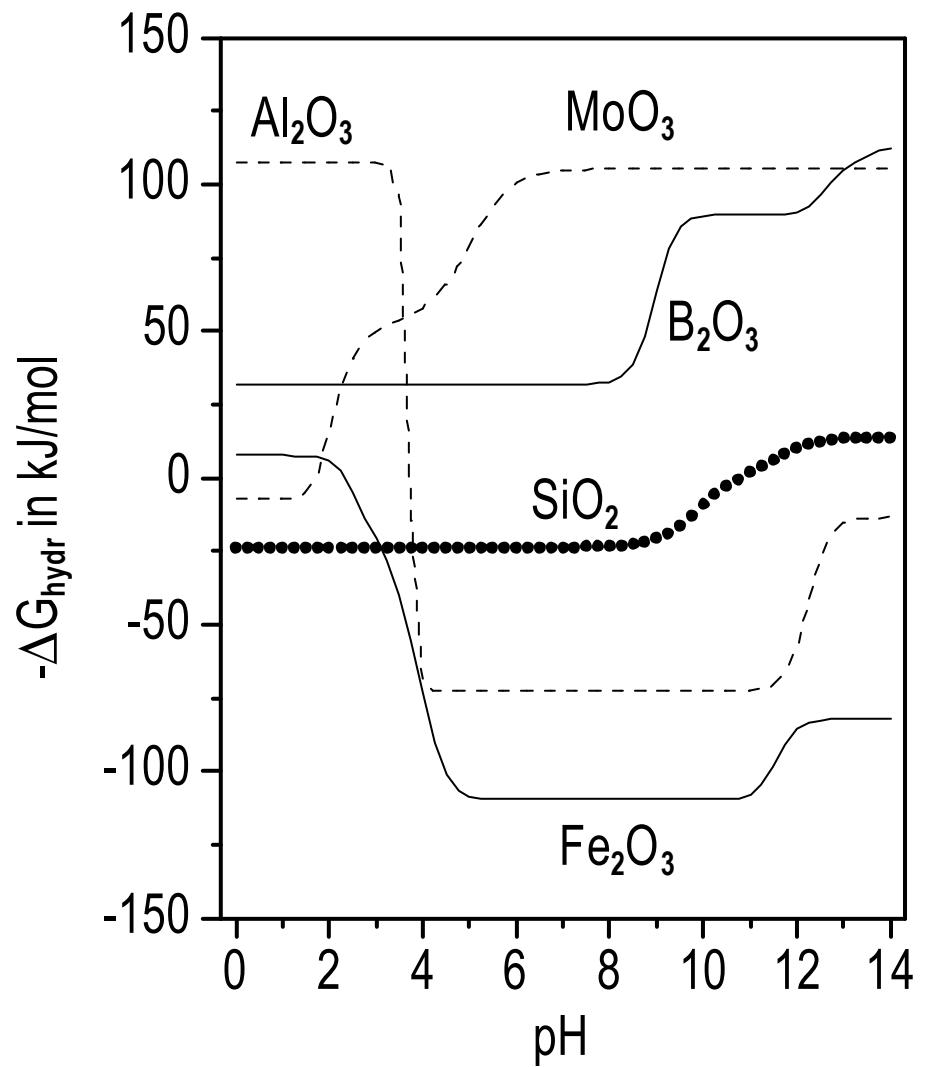
$$-RT \cdot \sum x_i \cdot \ln K_i$$











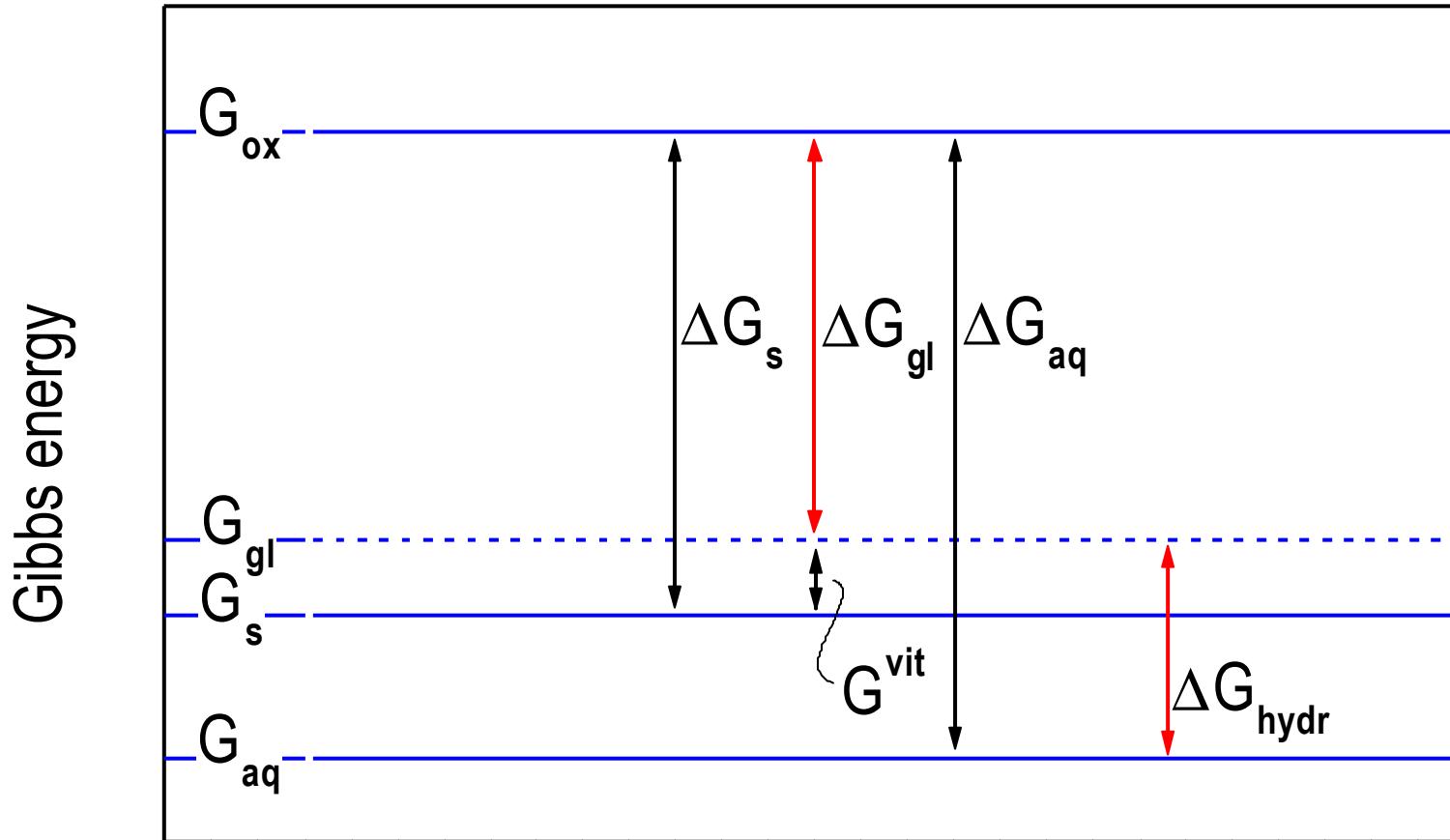
The state „dissolved in water“ is a state like the states „solid“, „liquid“, and „gas“. It is denoted by (aq).

$\text{SiO}_2(\text{aq})$ = silica dissolved in water.

*We may a glass like a „state“ - although it is not an equilibrium state like:
 $\text{SiO}_2(\text{gl})$ = silica glass.*

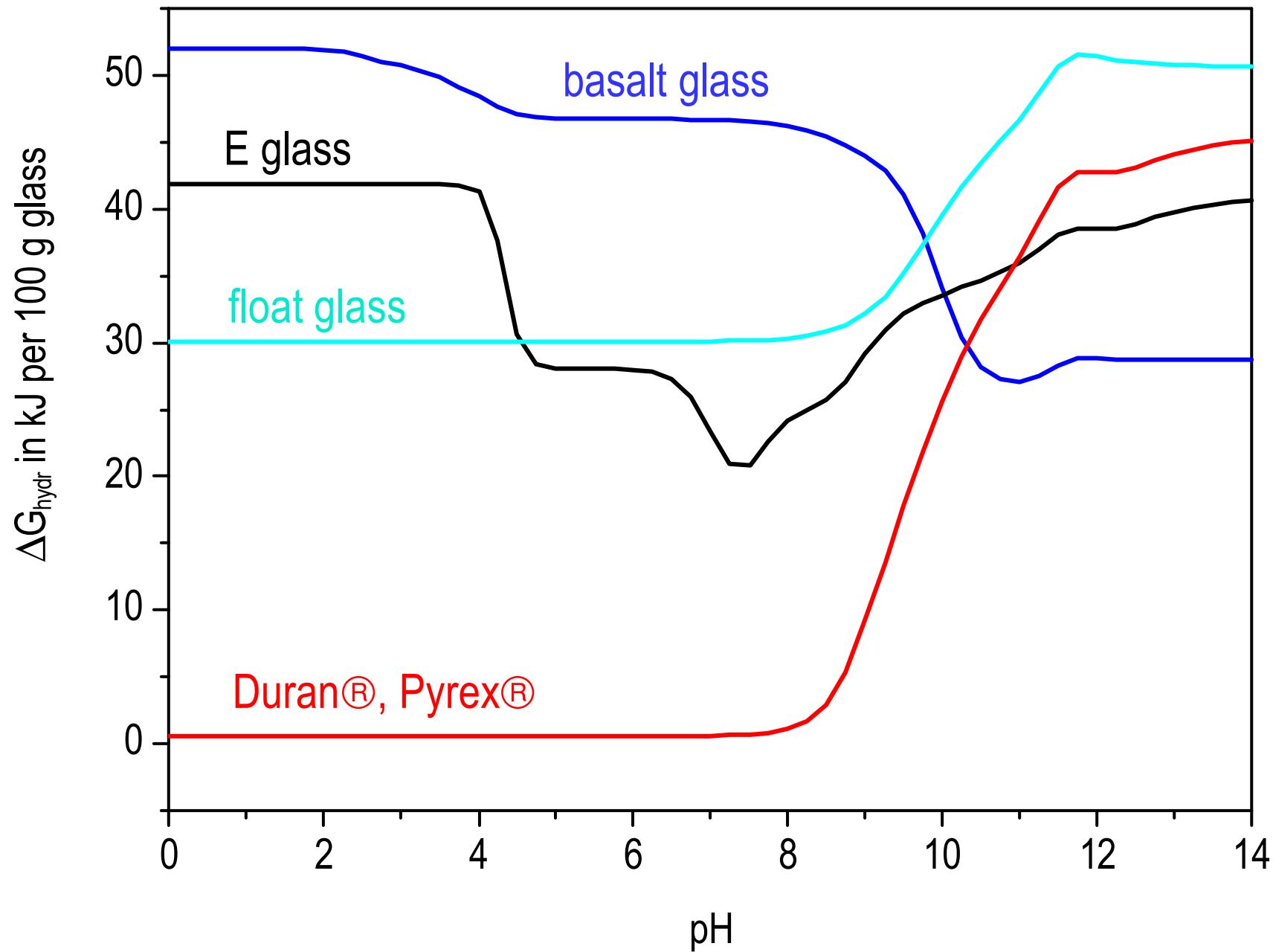
*Let us discuss a glass like
 $[74\text{SiO}_2 + 10\text{CaO} + 16 \text{Na}_2\text{O}](\text{gl})$*

*What state corresponds to
 $[74\text{SiO}_2 + 10\text{CaO} + 16 \text{Na}_2\text{O}](\text{aq})$?*



- (1) oxides + aqueous solution → aqueous species =
oxides → aqueous species – aqueous solution ⇒ ?G_{aq}
- (2) equilibrium compounds → oxides ⇒ -?G_s
- (3) glass → equilibrium compounds ⇒ -G^{vit}
- (4) glass + aqueous solution → aqueous species ⇒ ?G_{hydr}

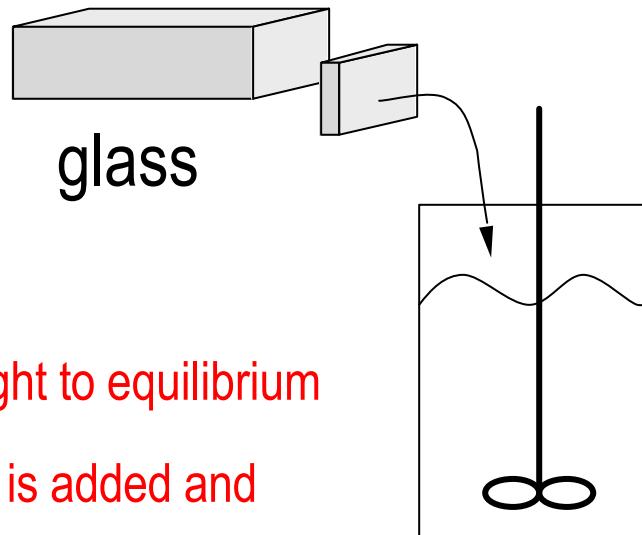
stability fingerprints of different glasses



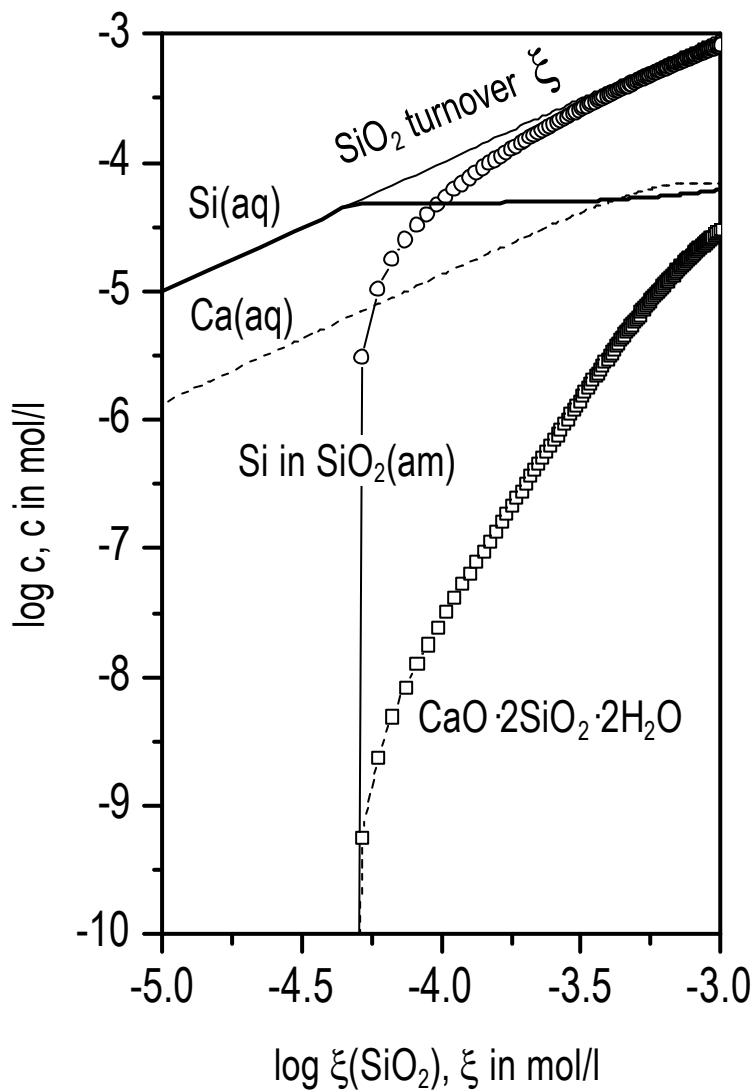
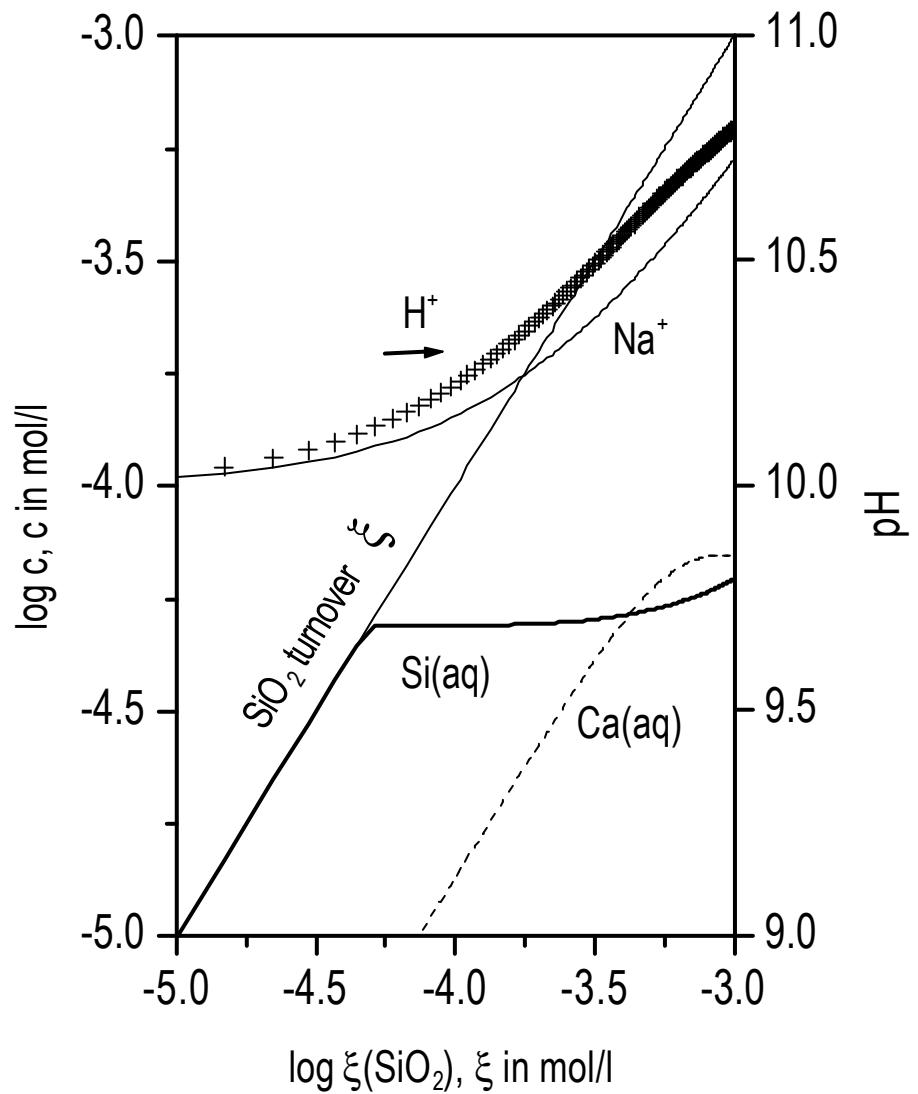
reaction path modeling

How to model the reaction path

[composition](gl) ® [composition](aq) ?



- A slice of glass is brought to equilibrium with the solution.
- The next glass slice is added and brought to equilibrium.
- The time scale is replaced by a sequence of glass slices.
- We learn towards what state the corrosion process moves.



mineralized glass,
amorphous and crystalline precipitates,
„back precipitates“, „transformed layer“

adsorbed layer

surface zone

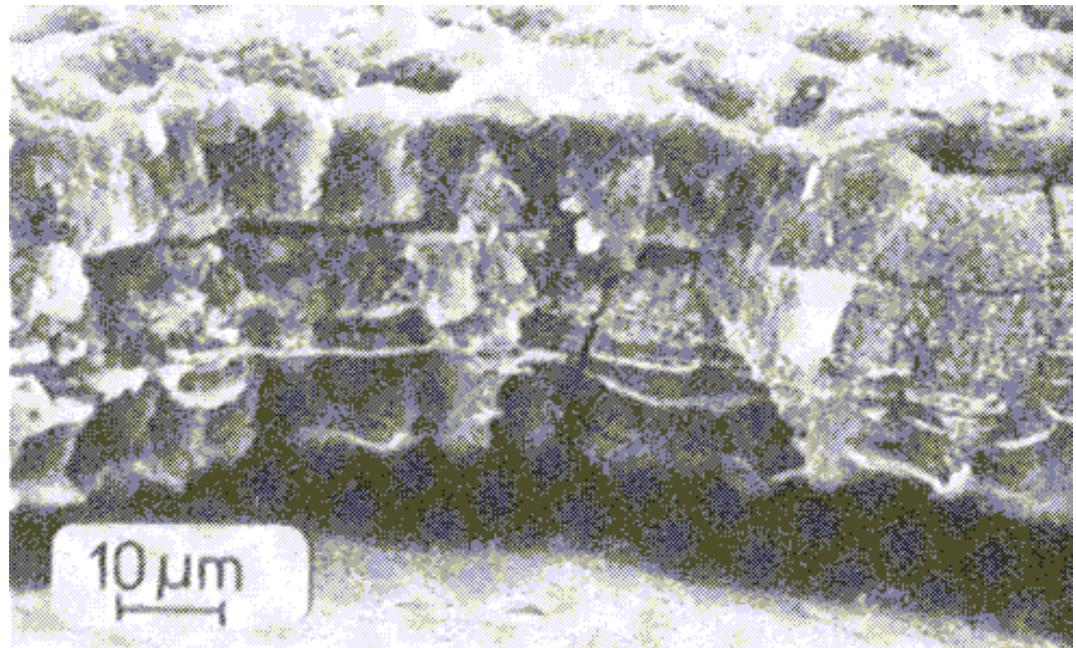
aqueous solution,
dissolved glass
components

bulk glass

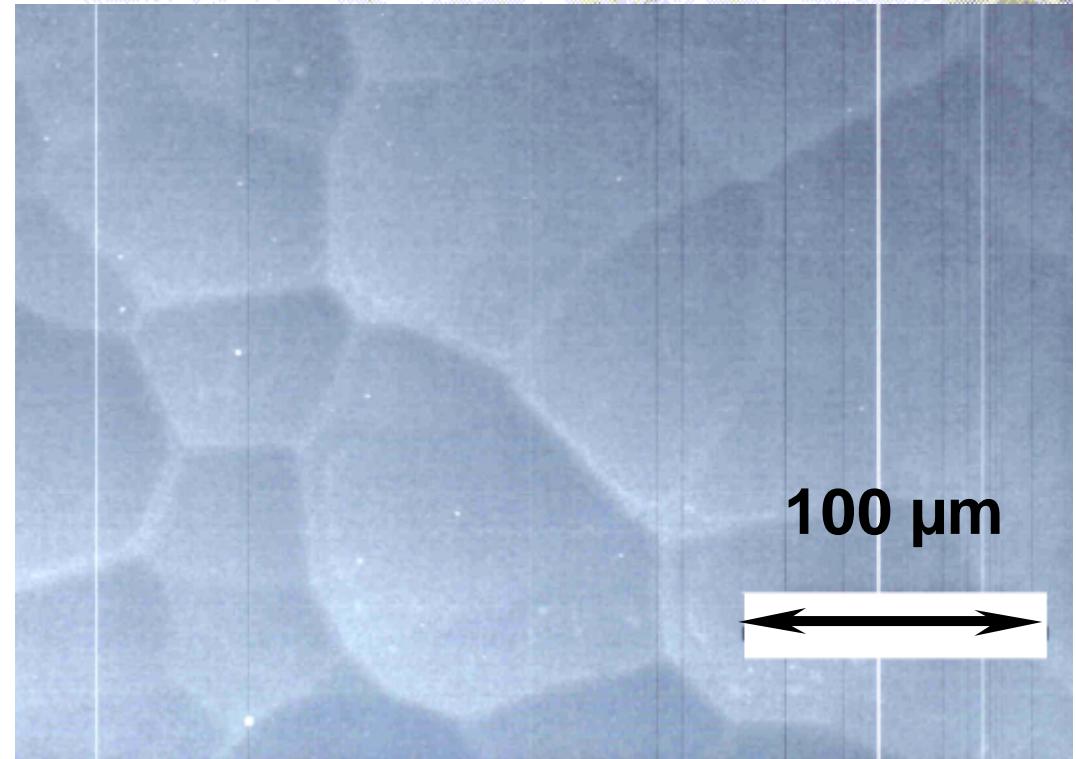
aqueous system

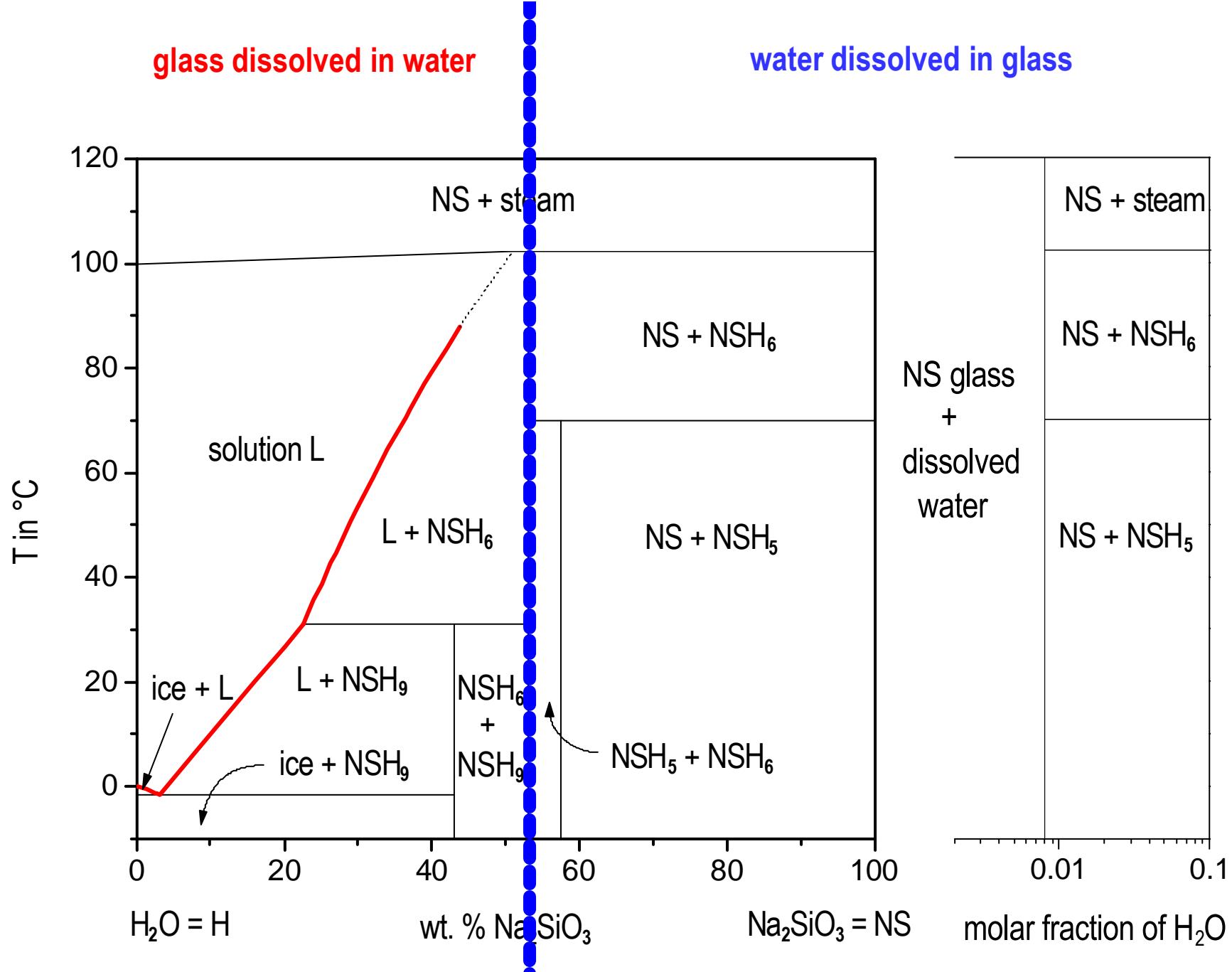
residual glass

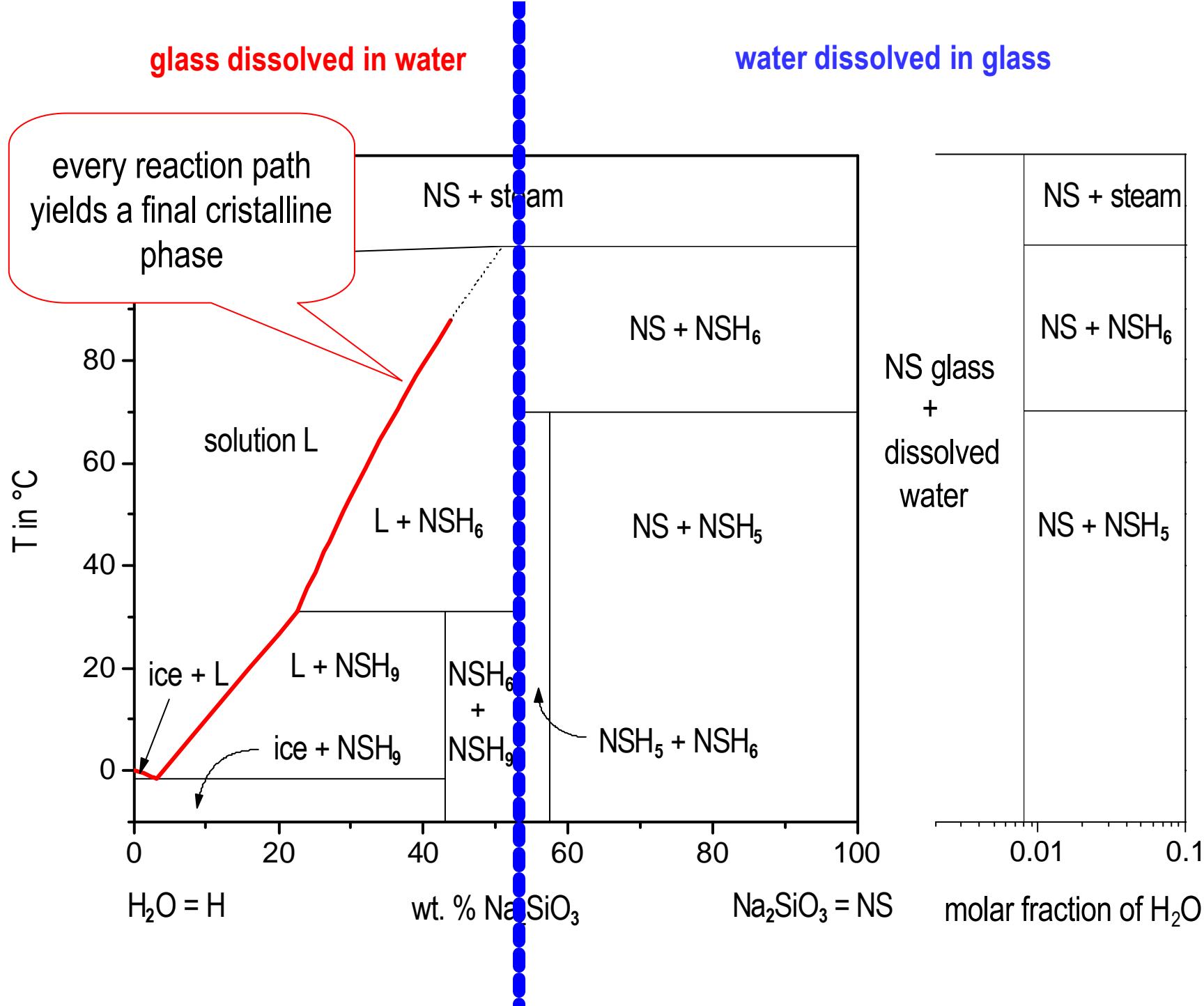
reaction product layer
(vertical section);



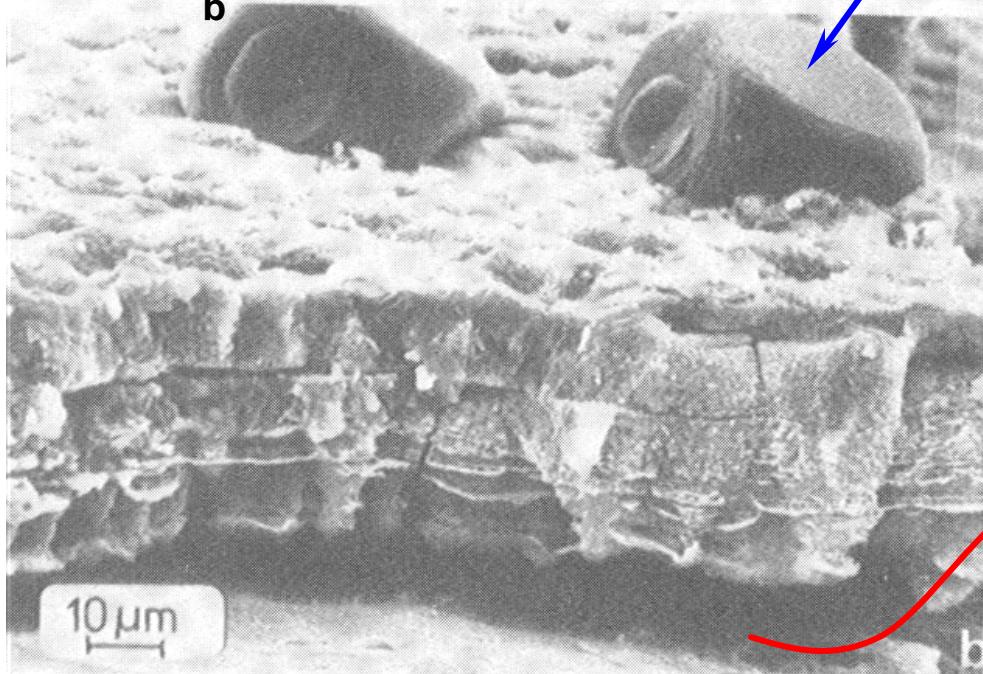
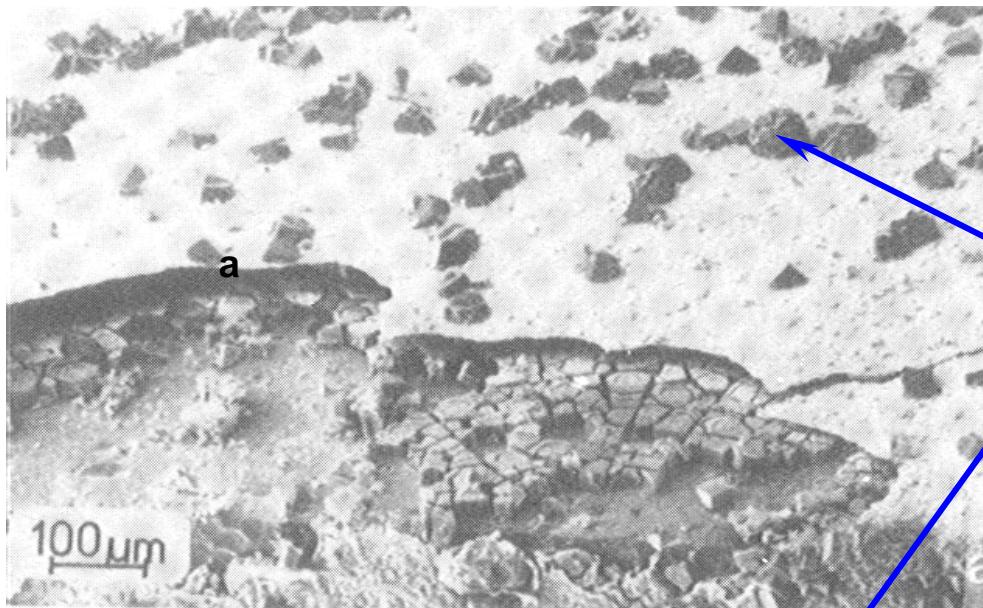
surface of the residual
glass after removal of
the reaction product
layer
(top view)







partially crystalline, partially amorphous layer of reaction products on top of the residual glass



G. Malow, W. Lutze, R.C. Ewing;
Stracchan; Chick & Pederson

analcime crystals:



$$\text{corrosion rate } r \rightarrow r_0 \cdot \left(1 - \frac{c_{ppt}}{c_s} \right)$$

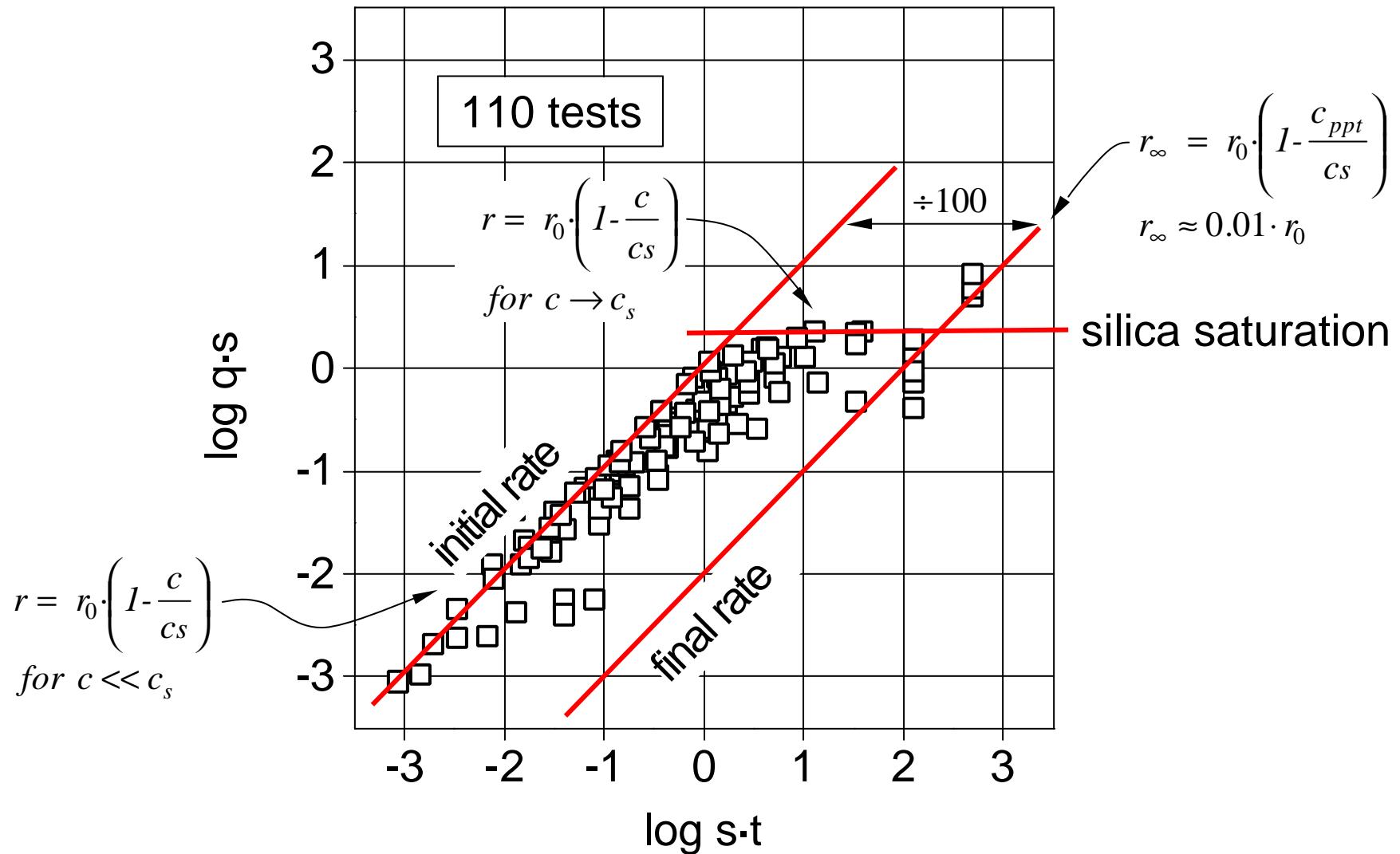
c_s = metastable solubility limit
of the glass;

c_{ppt} = solubility limit of the final crystal
formed along the reaction path

$c_s > c_{ppt} \Rightarrow r \text{ cannot reach zero}$

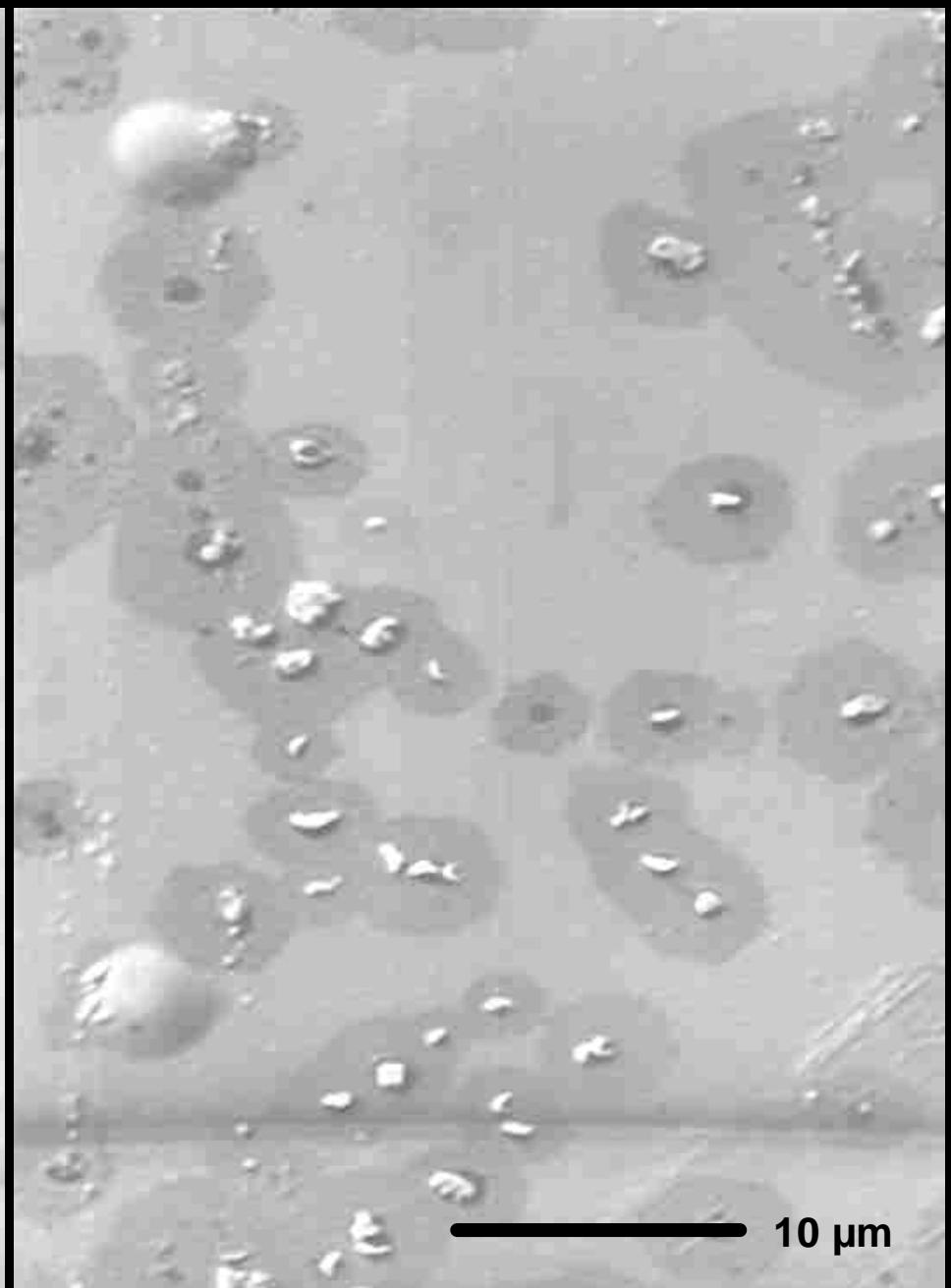
in many cases, the layer
can be removed easily
(like ice from a car windshield)

saturation with respect to the glass is a transient stage in most cases



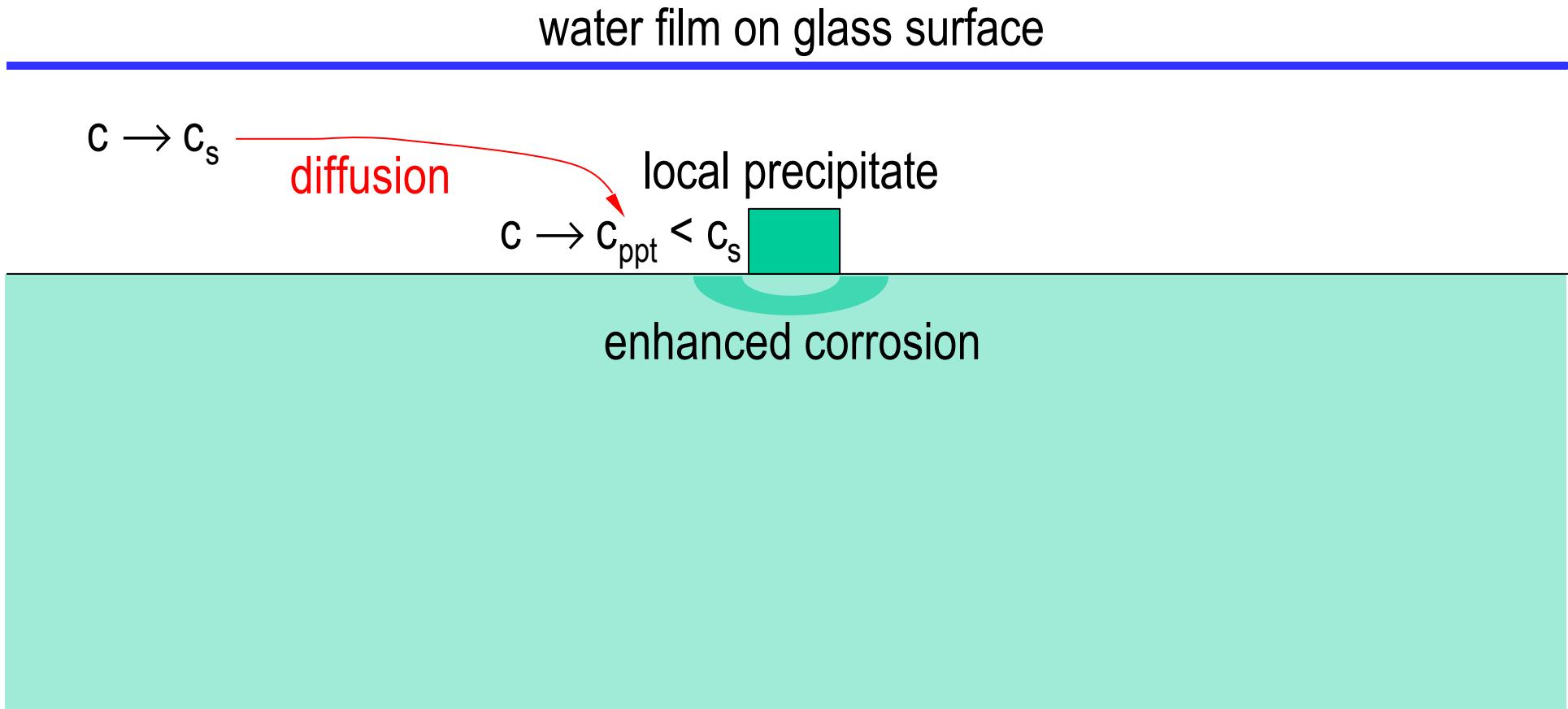
own work

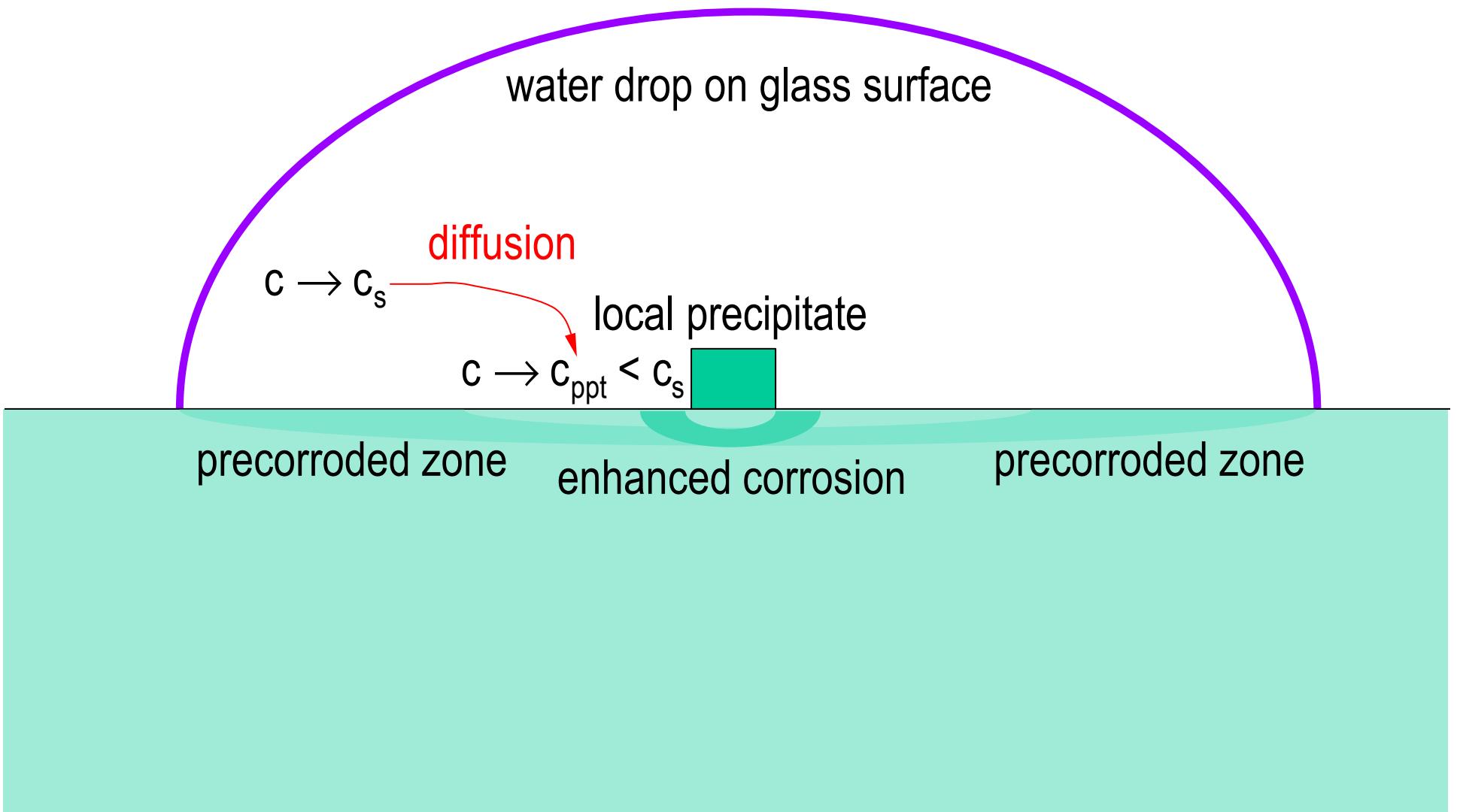
„soda bloom“ on OCEAN-Glas



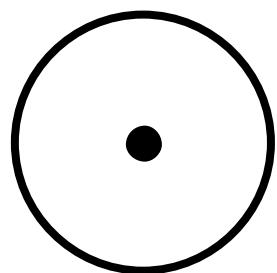
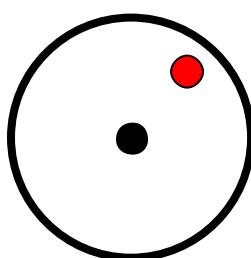
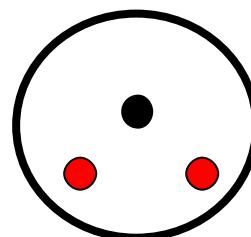
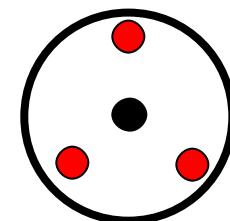
stage 1: due to large SA/V, pH → pH_s and c → c_s; $r_s = r_0 \cdot (1 - c / c_s) \rightarrow 0$

stage 2: eventually, a local ppt forms with solubility c_{ppt} < c_s; the rate in the vicinity of ppt is $r = r_0 \cdot (1 - c_{ppt} / c_s) > 0$. Thus, a „local element“ is generated.





*the nature of the sub-surface zone
and the rate determining step*

O^{2-}  OH^-  H_2O  H_3O^+ 

,“radius” 0.140 nm
d(O-H) -.-
 $\varphi(H-O-H)$ ---

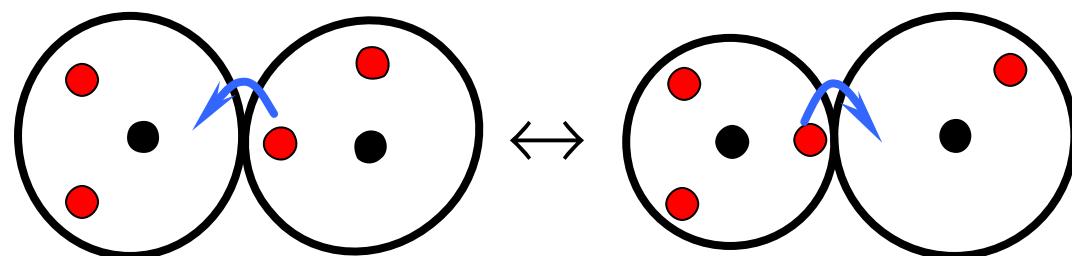
0.138 nm
0.096 nm

0.137
0.0958
104.45°

0.136
0.095
120°



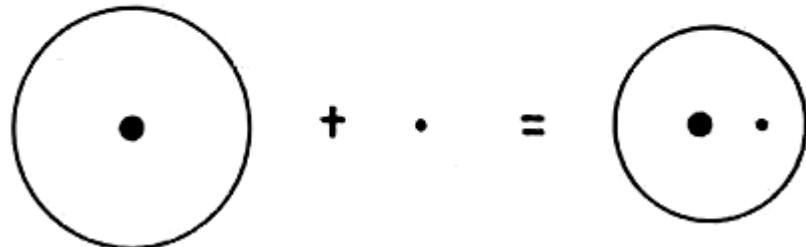
$$K_w = 10^{-14}$$



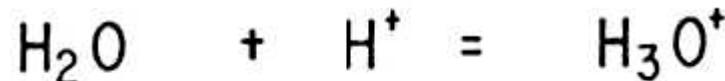
proton transfer!

H^+ is not an ion, but an elementary particle

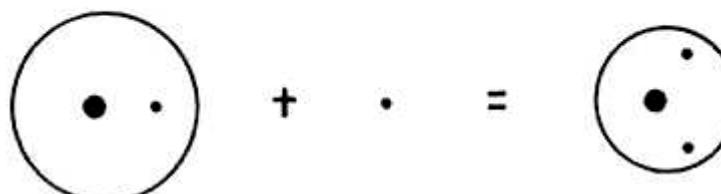
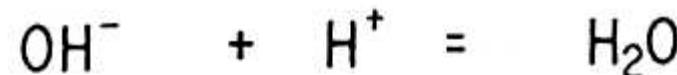
adsorption of proton by hydrogen:



adsorption of proton by water molecule:



adsorption of proton by hydroxyl ion:



Grotthuss proton transfer:

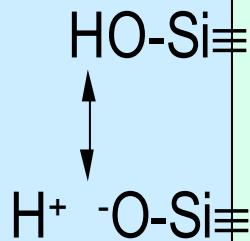


F.M.Ersnberger:

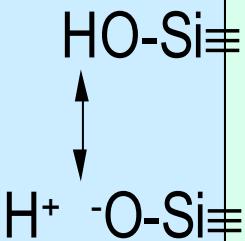
The Nonconformist Ion.

J. Am. Ceram. Soc. 66(1983)747-750.

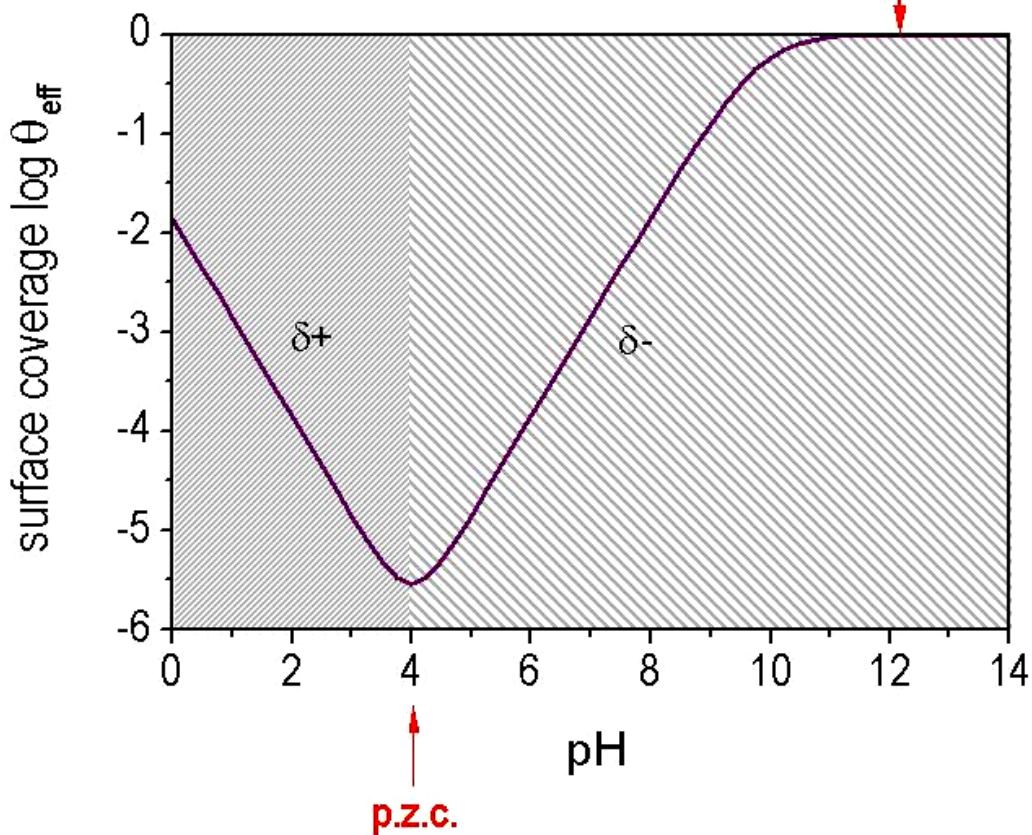
surface
equilibrium
Boksay 1980
Baucke 1996

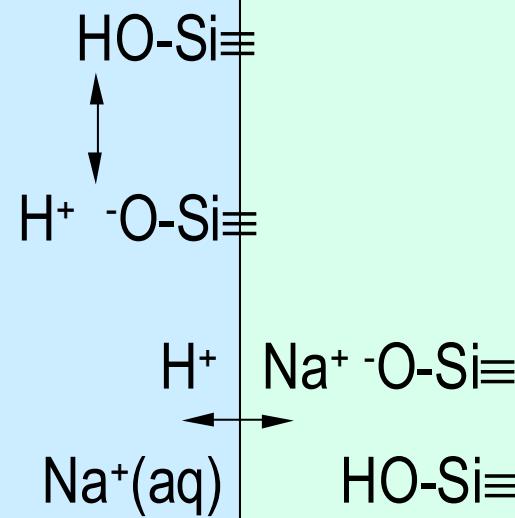


surface
equilibrium
Boksay 1980
Baucke 1996

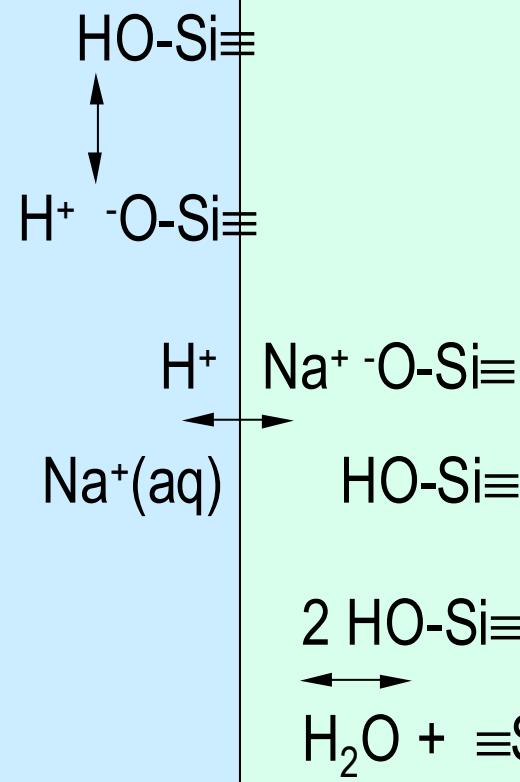


Schindler et al. 1976, compiled by Iler 1979:
5.5-5.8 OH groups per nm²

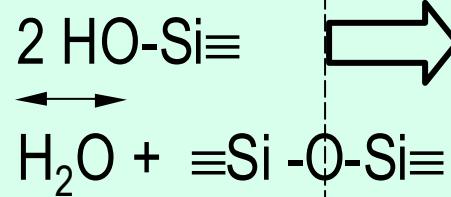
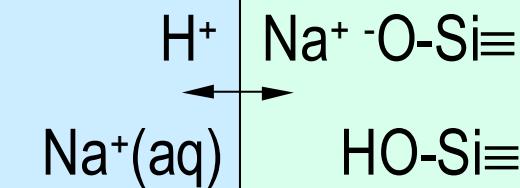
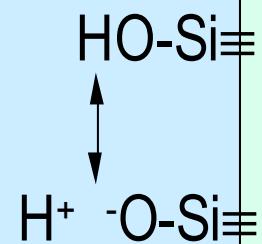




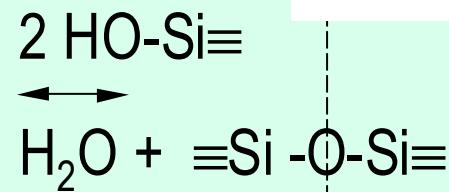
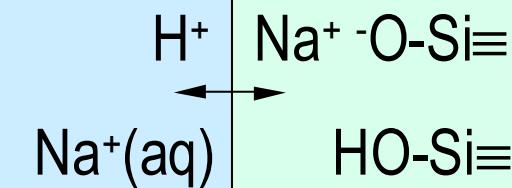
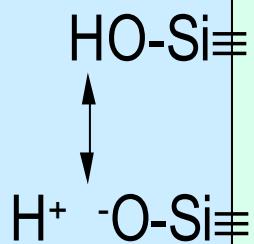
**proton transfer initiates
the mobilization of Na^+**



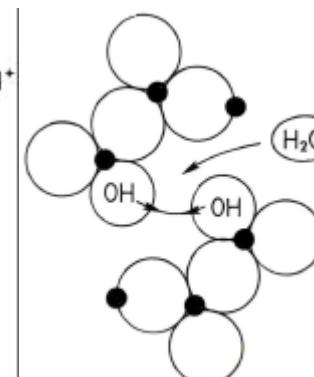
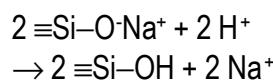
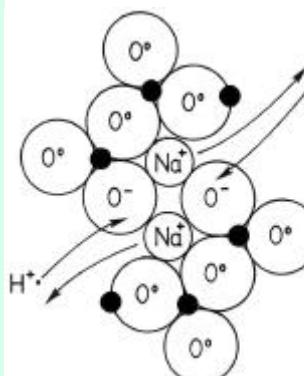
**reaction of OH to H_2O ;
condensation of silanol
to siloxane bonds ...**



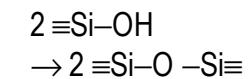
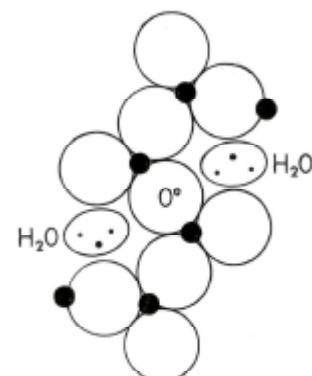
... generates and shifts
an inner boundary or
transition zone



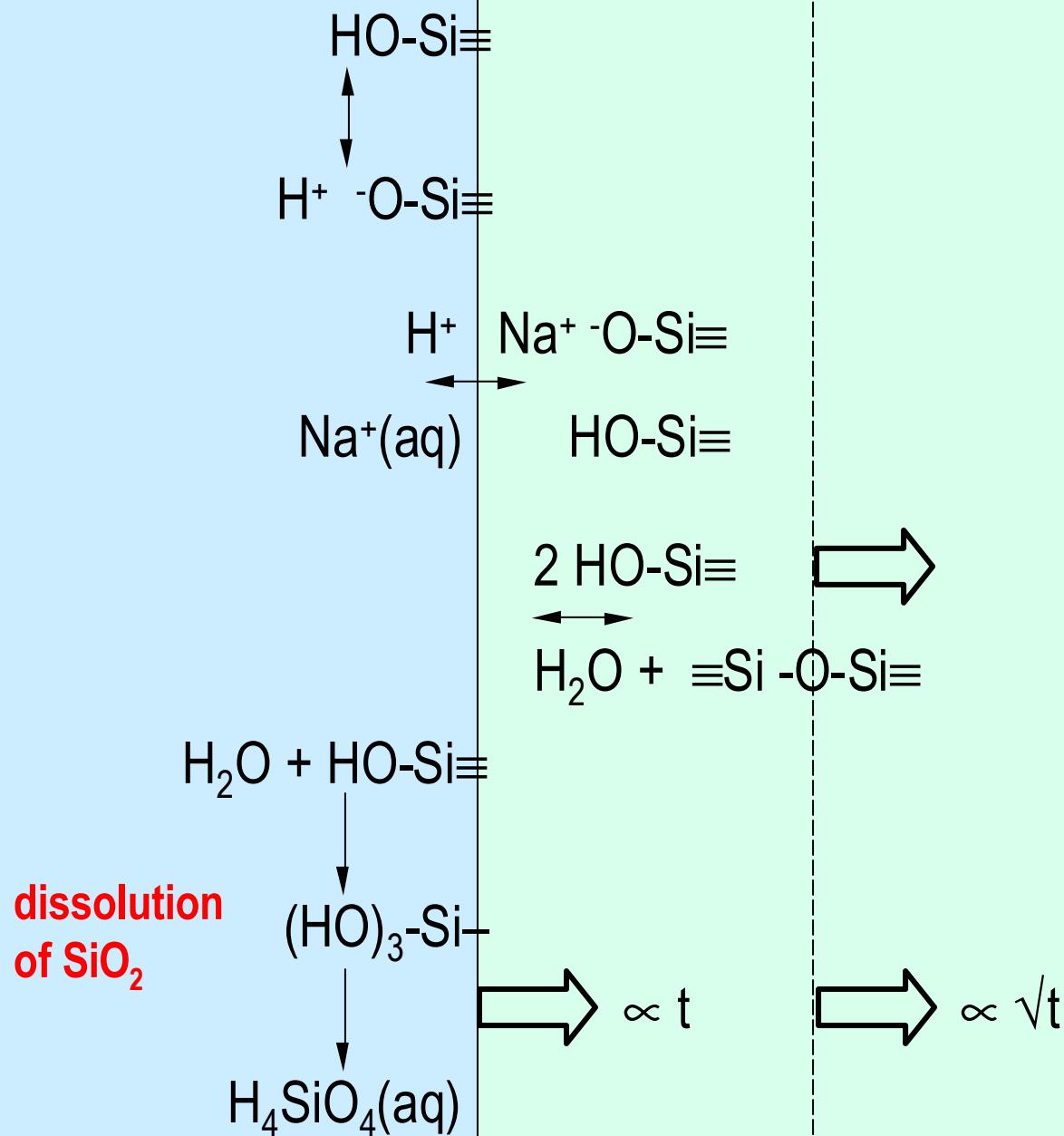
I. → II. → III.



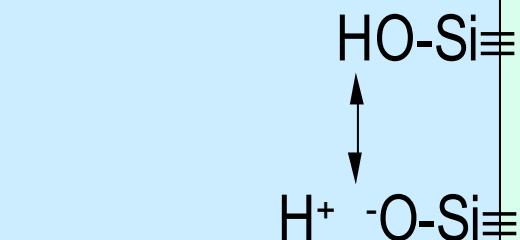
OH groups approach
each other; interstitial
water moves into void



$\longrightarrow \propto \sqrt{t}$

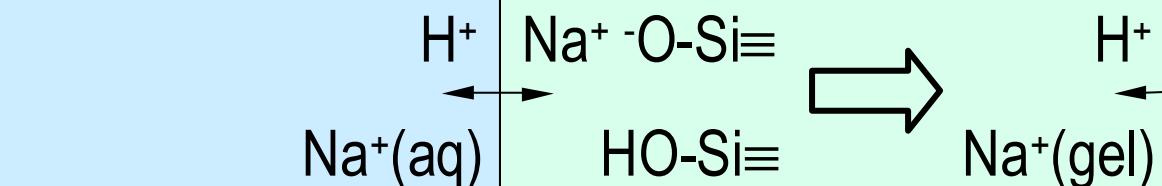


solution



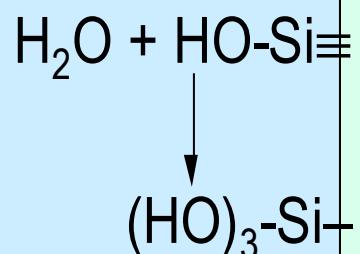
sub-surface zone

*low density,
high connectivity,
 H_2O percolation
high H_2O mobility*



$$D \approx 10^{-5} \text{ cm}^2/\text{s}$$

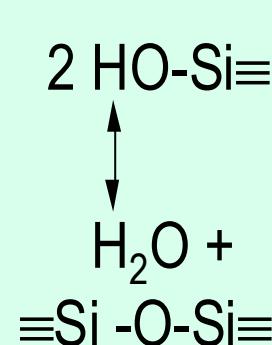
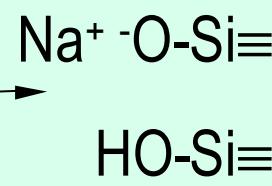
$D \approx 10^{-11} \text{ cm}^2/\text{s}$
fast exchange of
 $\text{H}^+, \text{Na}^+, \text{H}_2\text{O}$



*same kind of chemistry
like in aq. solutions;
in specific: dominance of
 H^+ controlled reactions*



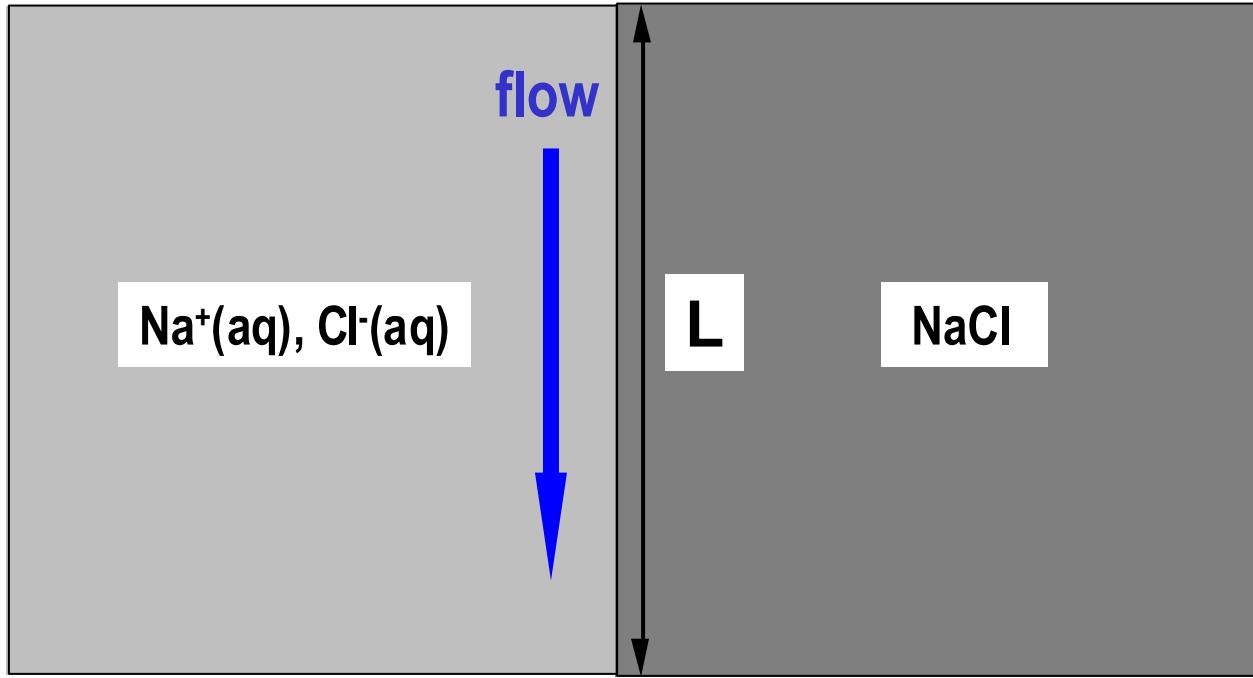
bulk glass



$$\longrightarrow \propto \sqrt{t}$$

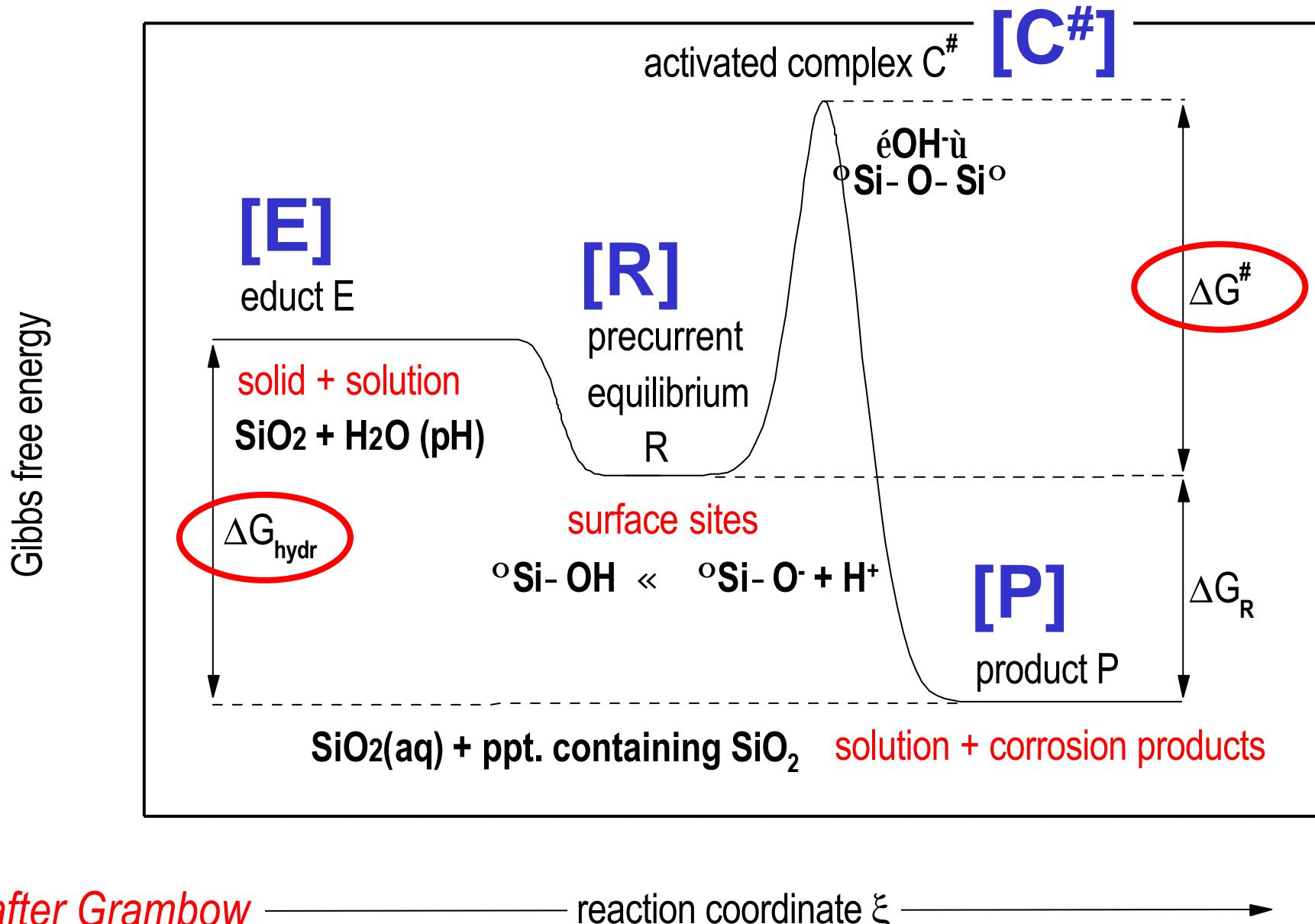
$$D \approx 10^{-14} \text{ cm}^2/\text{s}$$

rate control by fluid film diffusion: $E_A \approx 20 \text{ kJ/mol}$



$$r = \underbrace{\mathbf{b} \cdot (c_s - 0)}_{r_0} \cdot \left(1 - \frac{c}{c_s} \right), \quad \mathbf{b} = f(v, r, h, L)_{FLUID}$$

rate control by activated surface complex:
 $E_A \approx 70-80 \text{ kJ/mol}$



reaction velocity:

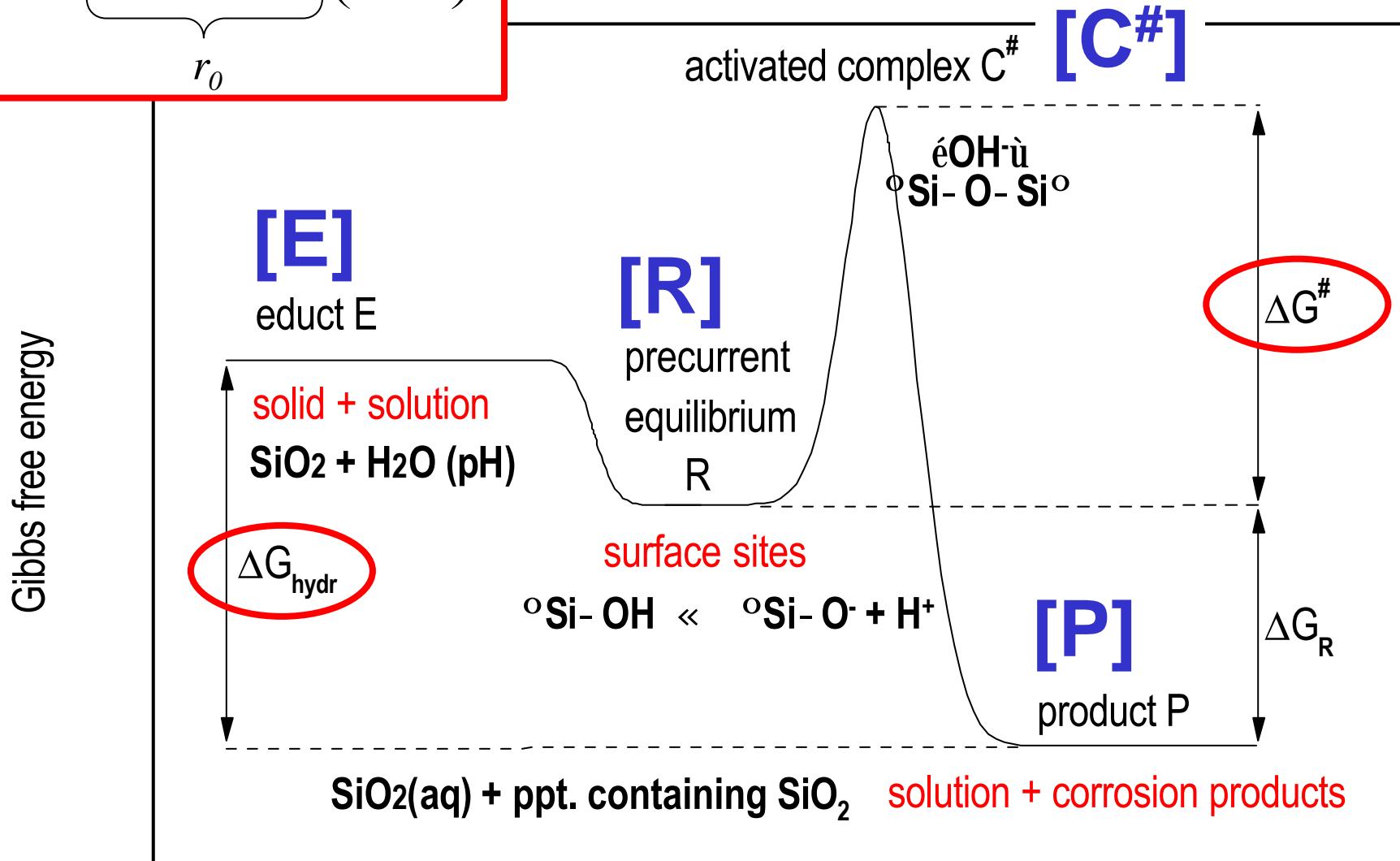
$$\begin{aligned} r = r_+ - r_- &\propto \exp\left(\frac{-?G^\#}{RT}\right) - \exp\left(\frac{-?G^\# - ?G_{hydr}}{RT}\right) \\ &\propto \exp\left(\frac{-?G^\#}{RT}\right) \cdot \left[1 - \exp\left(\frac{-?G_{hydr}}{RT}\right)\right] \approx \exp\left(\frac{-?G^\#}{RT}\right) \cdot \left[1 - \frac{c}{c_s}\right] \end{aligned}$$

linear free energy relationship (LFER):

$$?G^\# \propto ?G_{hydr}$$

$$r = \underbrace{\mathbf{b} \cdot \frac{kT}{h} \cdot [C^\#]}_{r_0} \left(1 - \frac{c}{c_s} \right)$$

rate control by activated surface complex:
 $E_A \approx 70\text{-}80 \text{ kJ/mol}$



after Grambow

reaction coordinate ξ

thermochemical rate equation

LFER

$$\log r = \log r_x - \frac{E_A}{RT} - b \cdot \log q - \frac{e \cdot ? G_{hydr}(\mathbf{x})}{RT} + \log \left(1 - \frac{c(\mathbf{x})}{c_s} \right)$$

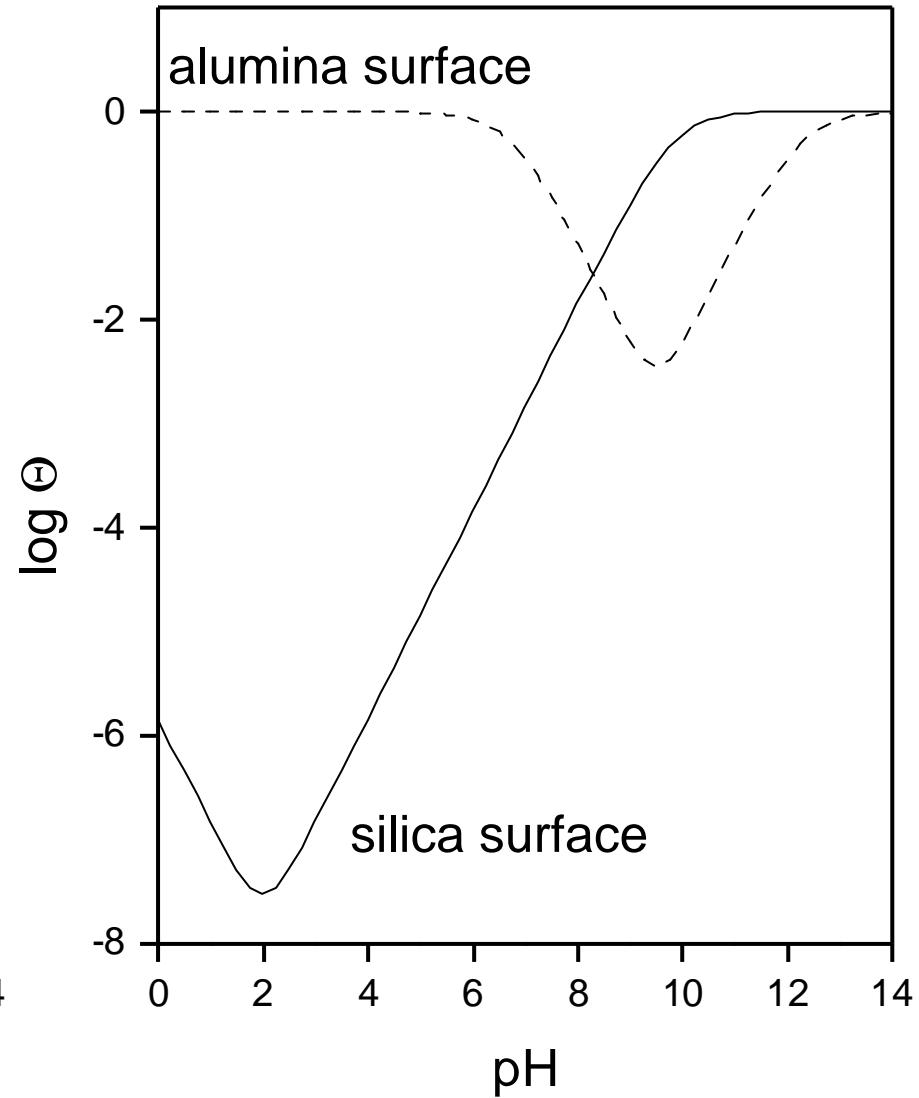
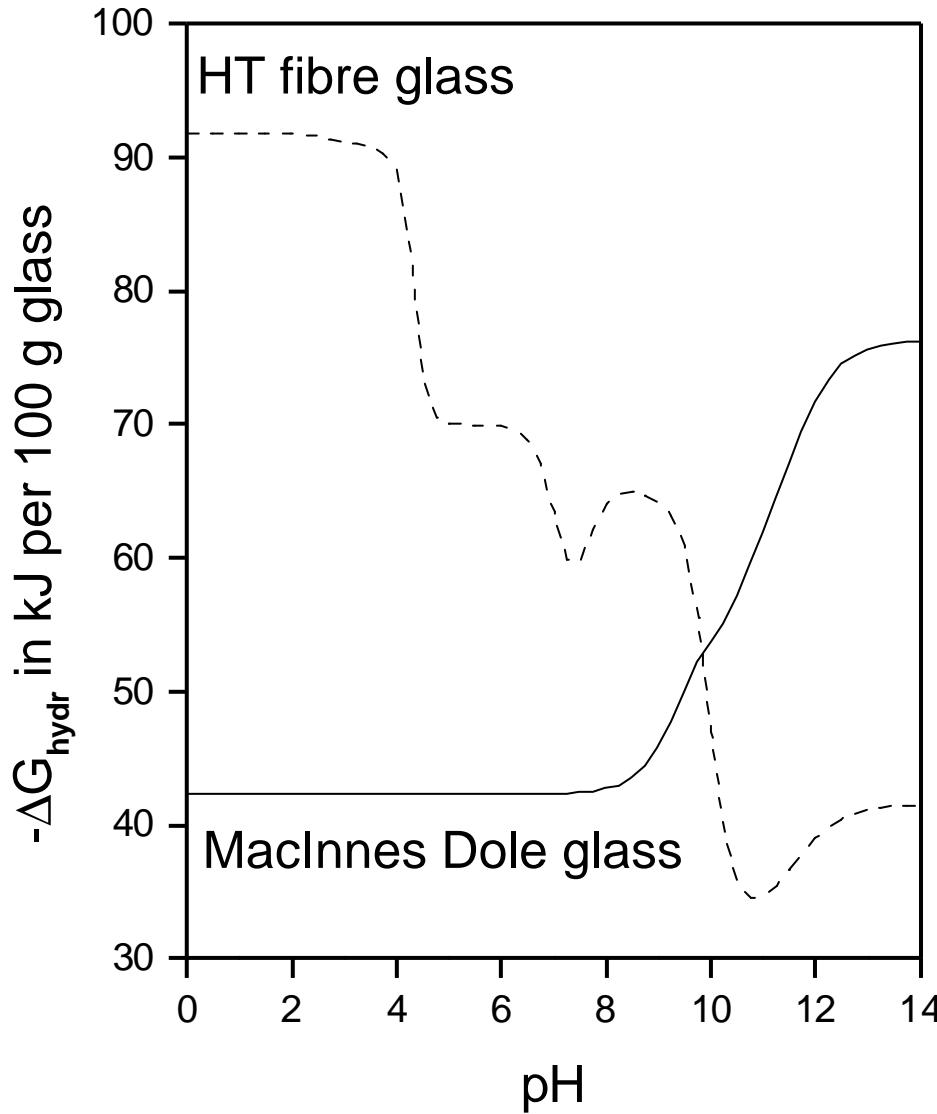
molecular dynamics

surface
equilibrium

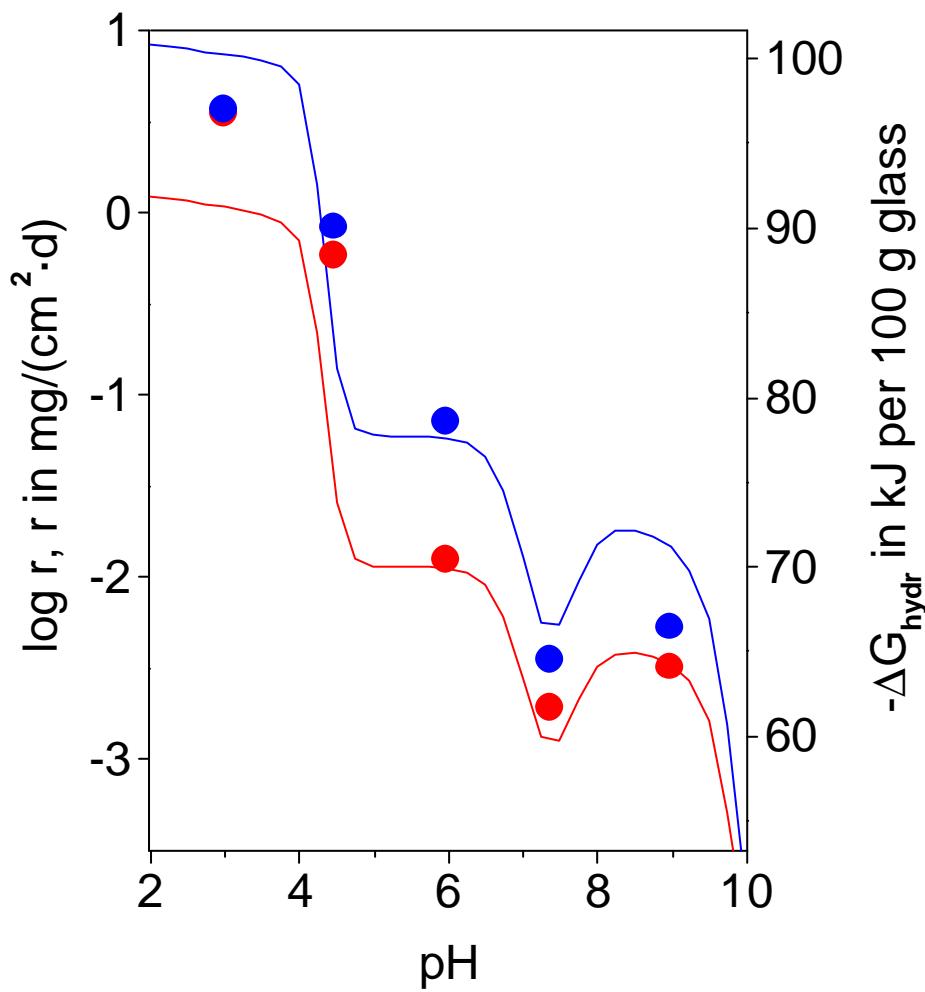
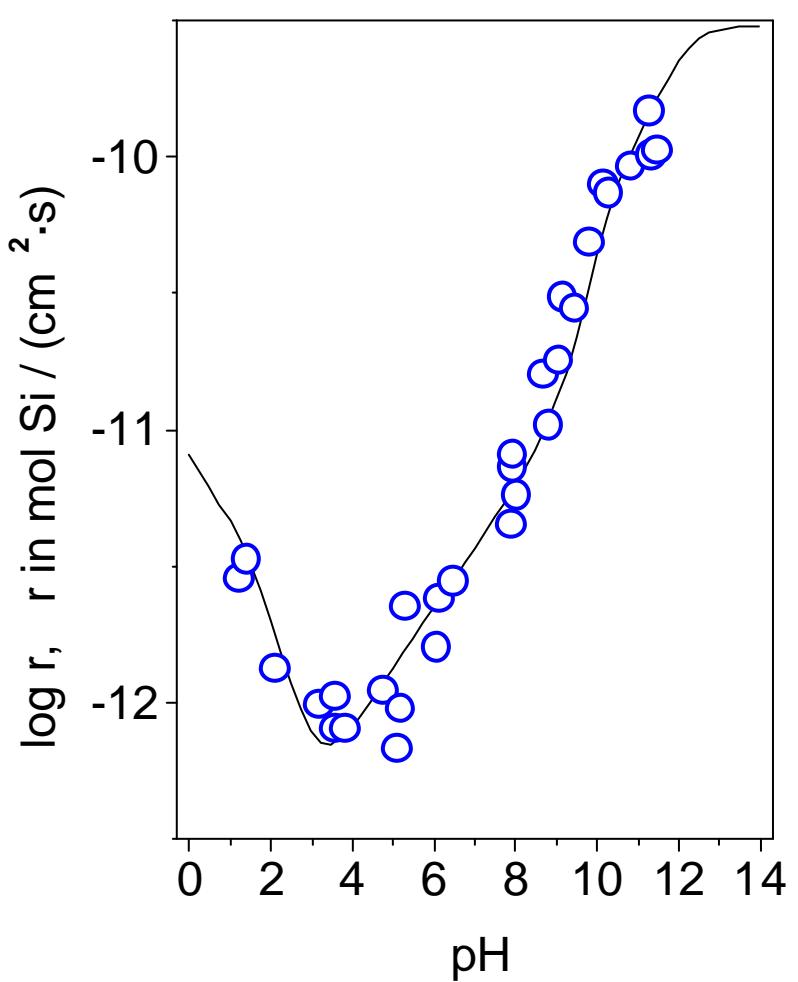
glass
chemistry

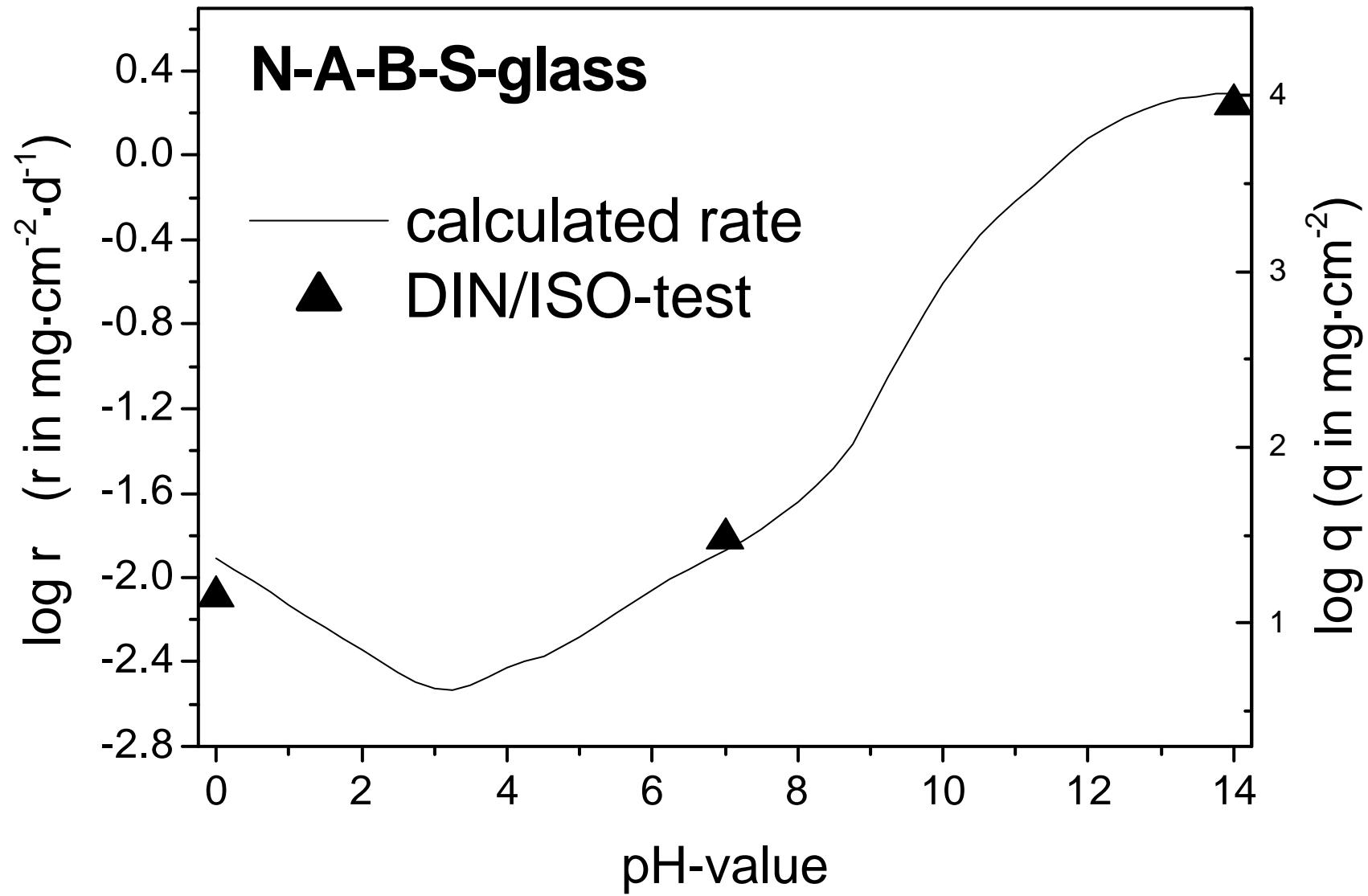
saturation;
long term
exposure

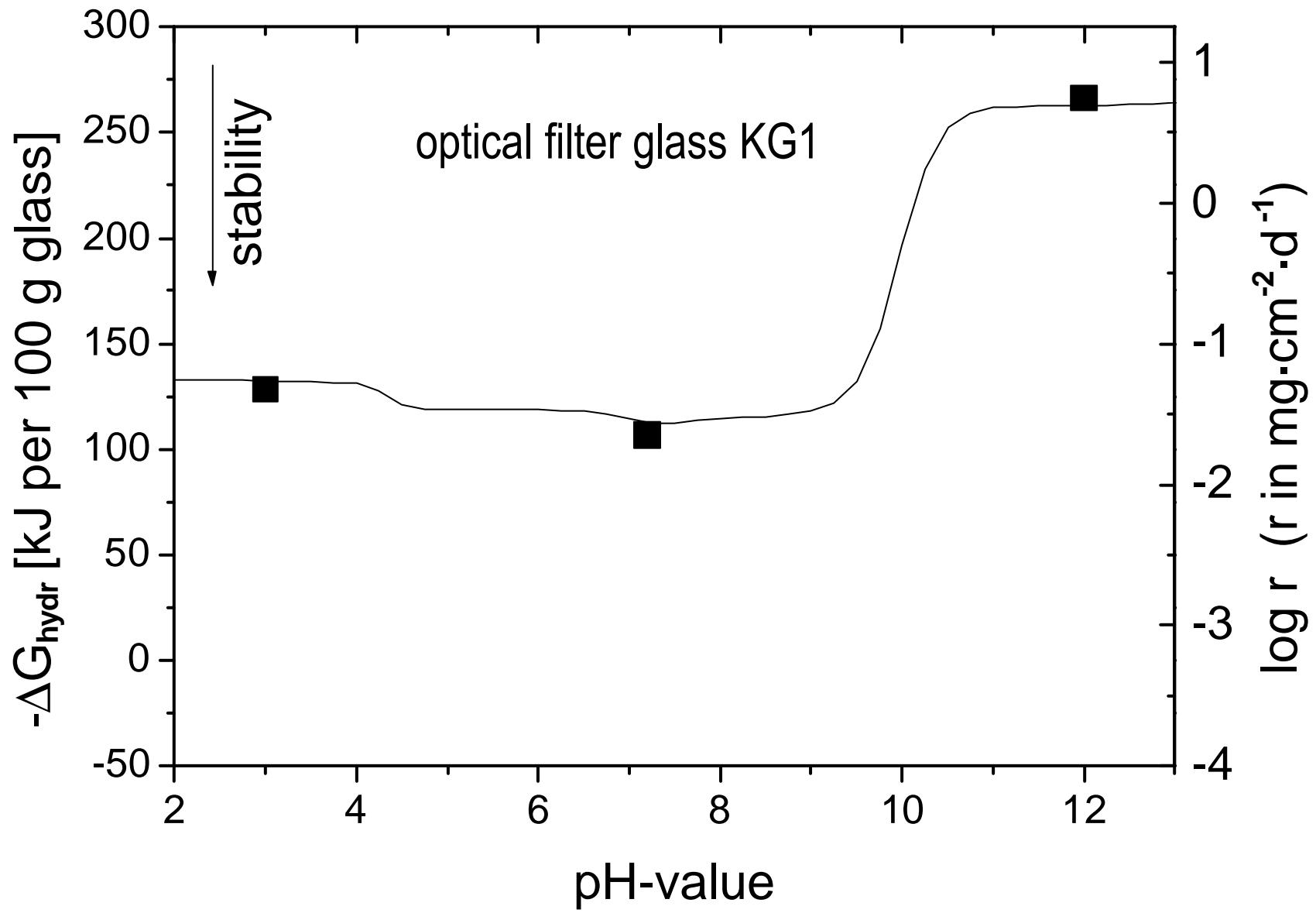
Corrosion rates at high water excess (low s parameter) :
 „Multiply“ the stability fingerprint or solubility (left graph) with the surface coverage (right graph) ...



... and obtain a prediction of the dissolution rate as $f(\text{pH})$.



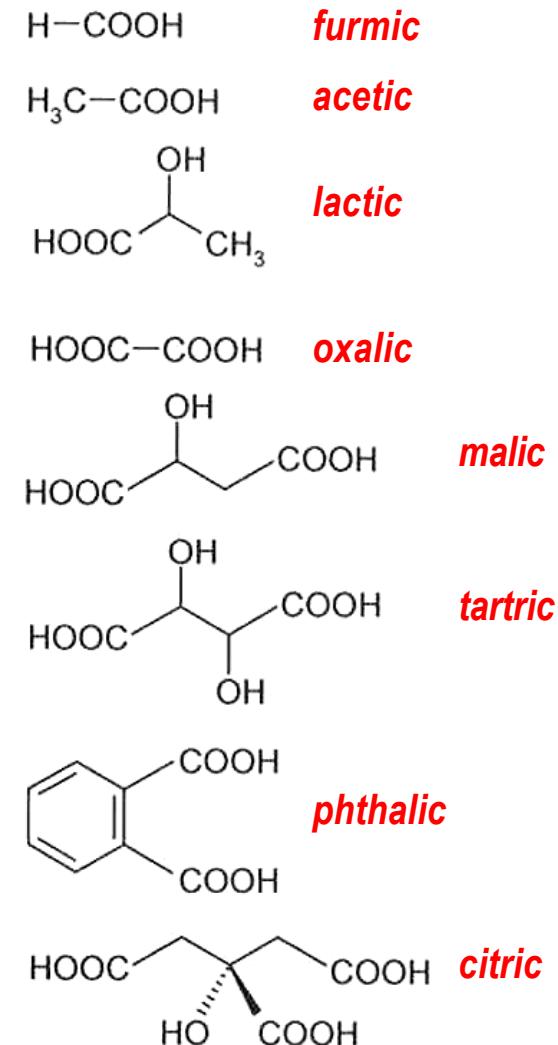
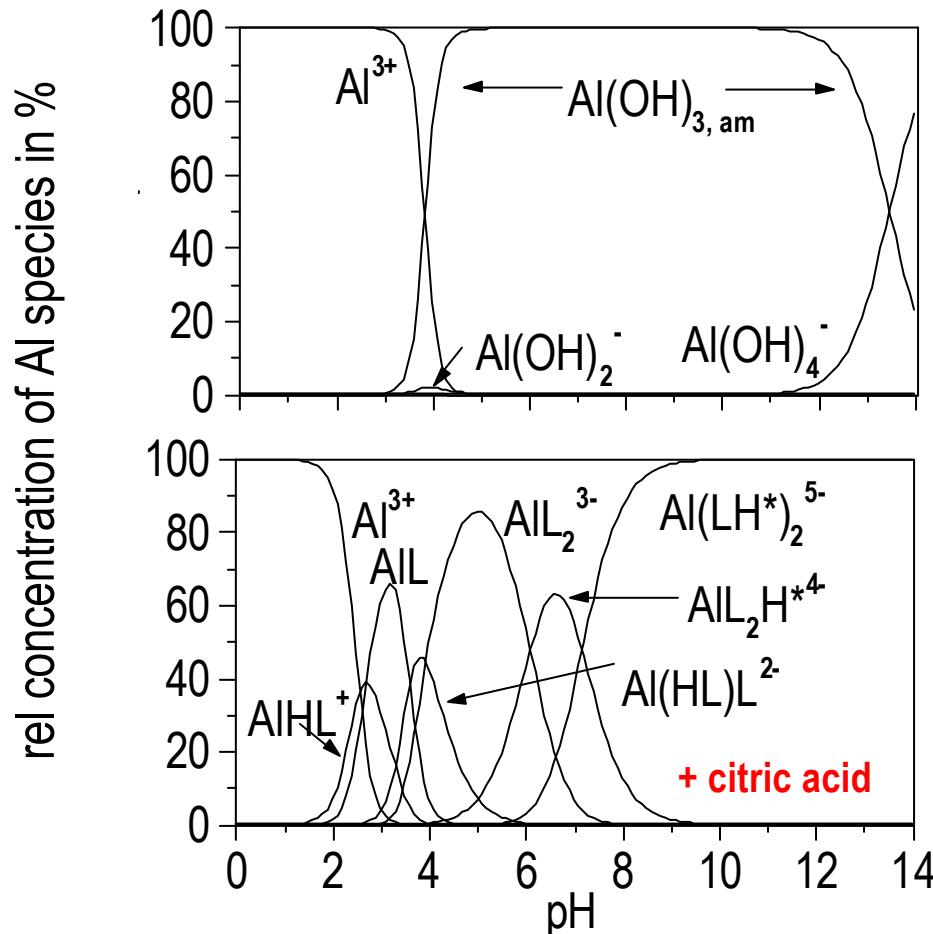




Interaction between organic components and glass – a key to applications in medicine and biotechnology

two key mechanisms:

- influence on the solubility,
- influence on the surface equilibrium.



Thank you
for your
kind attention!